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Trajectory Reconstruction and Aerodynamic Results from the First Discovery Flight, STS-14(41-D)

IN-16

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ABSTRACT

Trajectory reconstruction results for the first Discovery flight are presented. Spacecraft dynamic measurements from IMU2 were utilized in conjunction with the ground based tracking data from two S-band stations, eight C-band, and five cameras at Edwards Air Force Base to determine the spacecraft trajectory from epoch through rollout on Runway 17. Specifics as to the trajectory reconstruction are discussed in Section I herein. The final inertial profile is BT14N02/UN=169750N. Merging of this file with the final LAIRS atmosphere is discussed in Section II. The final Extended BET is ST14BET/UN=274885C. Section III presents plots of relevant parameters from the AEROBET as well as aero-dynamic performance comparison results. High frequency files for maneuver extraction were also generated as discussed in Section IV.

The following table is presented as summary information for STS-14 (41-D):

(Epoch: $9/5/84 12^h 59^m 0^s (46740^s) GMT_h_0 = 669 kft$)

Event	Time from epoch	Altitude (kft)
Entry interface	480	400
Initial flight extraction	629	320
Maximum Mach (28.0)	718	277
M25	938	241
M20	1242	218
M15	1428	192
M10	1584	169
M5	1798	122
M2	1975	77
M1	2069	50
Main gear deployment	2314	2.3
Weight on wheels	2333	2.1
Weight on nose	2345	2.1
Stop time	2399	2.1

Appendices are attached which contain (A) spacecraft and physical parameters utilized, (B) final residuals obtained from the data fitting process, (C) listing of trajectory parameters, and (D) archival information.

I. Entry Trajectory Reconstruction

I.a. Dynamic data

IMU2 was selected as the dynamic data source for the STS-14 entry reconstruction. Figure I-1 shows the dynamic data time history over five hundred(500) second intervals starting at 0 seconds (~669 kft). Body axes rates and accelerations derived from the IMU2 measured $\Delta V_{\mbox{\scriptsize M50}}$ and quaternions are plotted.

In terms of the total sensed ΔV magnitude, the tri-redundant IMUs agreed very well. IMU1 and IMU2 agreed to within 0.44 fps while IMU3 was within 0.32 fps of the other two. Mid-value selection (percentage of occurrences) for the various units are shown in the following two tables:

Accelerometer Comparisons Based on 2415 Points

	Percenta	ge mid-value	measurement
	IMU1	IMU2	IMU3
$^{\Delta V}$ X _{M50}	7	29	64
ΔV _Y M50	28	7	65
MSO ΔV _Z MSO	25	49	26

Gyro Comparisons Based on 2420 Points

	Percentage	mid-value	measurement
	IMU1	IMU2	IMU3
Euler ψ	15	81	4
Euler θ	29	51	20
Euler φ	0	58	42
Total angle,	Γ 28	48	24
Total angula	r 31	32	37
rate, Γ			

No clear choice is evidenced by these results. Arbitrarily, IMU2 was selected. No data gaps of over 4 seconds were detected in the Operational Instrumentation (OI) recorded data.

I.b. Tracking coverage

Tracking data for STS-14 were obtained from two(2) S-band radars (Guam, Goldstone), eight(8) C-band radars, and five(5) cinetheodolite cameras in the vicinity of Runway 17 at Edwards. Unfortunately, due to a mixup, the GSFC tracking tape contained no high rate (10/sec) data from Guam. Since the recorded high rate data are only kept by the station for approximately one week, a follow-up request for these data could not be satisfied. Therefore, low rate (1/10 sec) range and angle data obtained via the JSC were utilized for trajectory reconstruction. Low rate Guam Doppler data were not processed because of the instantaneous formulation for Doppler observations in ENTREE. Other tracking data excluded from the reconstruction process were: (1) C-band pass from Hawaii (KPTC) because of sparse, low elevation (~4° Max) coverage; (2) Noisy range and azimuth data throughout the first half of the pass from Edwards (EAFC).

Figures I-2 and I-3 illustrate the tracking coverages for STS-14. Figure I-2 shows the entire entry ground track with stations (complexes) as noted. Times and corresponding altitudes at 500^{S} increments along the track are given. Figures I-3a, I-3b, and I-3c show the detailed tracking coverage from entry to California C-band acquisition, California C-band acquisition to final approach, and final approach to landing, respectively. Times, altitudes and station coverages with respect to the ground track are as shown. Acronyms and locations for the STS-14 trackers are given in Table I.

I.c. Reconstruction results

The final BET solution for STS-14, BT14N02, is presented in Table II. For comparison, the initial estimate from the onboard navigation system, the JSC/TRW estimate and a state-only ENTREE estimate are also given. Comparison of the two ENTREE estimates shows that a significant improvement in the fit to the tracking data is achieved by extending the solution set to include accelerometer scale factors. The estimates for scale factor corrections (+5, +107, +18 ppm in X, Y, Z, respectively) are consistent with the 10 performance specification levels of 100 ppm in each channel. There is very good agreement between

the JSC/TRW and BT14N02 solutions both at epoch and throughout the entry trajectory. The weighted fit statistics for BT14N02, based on 5783 observations, are μ_{W} = -0.118 and σ_{W} = 1.344. A summary of the residuals, by station and data type, is given in Table III. Plots of the final residuals are given as Appendix B. Composite residuals are included in this section. The symbol key for the stations appearing on the composite plots is given as Figure I-4. Composite range, azimuth and elevation residuals are shown as Figures I-5, I-6, and I-7, respectively.

Comparisons of the final BET position and velocity after rollout on Runway 17 versus post-landed survey values are given below:

END CONDITIONS AT VEHICLE STOP (Runway #17 Coordinates)

	Survey	BT14N02
X, ft	+12793	+12848
Y, ft	+66	+61
h-h _{RW} , ft	+16	+7
X, fps	0	+0.05
Ÿ, fps	0	-0.05
h, fps	0	-0.13

Figure I-8 presents plots of the BET during rollout on Runway 17. Surveyed values are depicted thereon. Vehicle stop occurs 2399^{S} after epoch.

TYPE	ST NO.	STATION NAME	LATITUDE (GEOD.) (DEG)	LONGITUDE (DEG)	ALT (ABOVE REF.) (FT)	MODULUS OF REFRACTION	SCALE HEIGHT (M)
BAND, N.S.	-	GWMS	13, 31063	144.73681	380.4100	380.	5795.
-BAND FPO-6	٠ ٨	PTPC	37-49784	237,50039	-27.0300	334.	6821.
C-BAND, TPO-18	۰ ۲	VDBC	34,66587	239,41865	203.5433	338.	6507.
-BAND, FPS-16	. v	VDSC	34.58276	239.43853	1972.1457	319.	.6040
THEODOLITE	. 9	THEO1	34.91673	242,29058	2742.4000	N/A	N/A
HEODOLITE	7	THEOS	34,83905	242,29574	2701.7400	N/A	N/A
THEODOLITE	. on	THE09	34.94739	242.08924	2370,2200	N/A	N/A
-BAND, FPS-16	σ	FRCC	34,96083	242.08856	2480.3478	299.	7387.
-BAND, FPS-16	, 0	EAFC	34.96962	242.06974	2521.7192	299.	7366.
HEODOLITE	-	THE 07	34.92839	242,23770	2378,5000	N/A	N/A
-BAND. N-S	12	GDSS	35,34221	243, 12654	2994.4600	289.	7556.
-BAND, FPO-14	7	KPTC	21,57210	201.73343	931,4000	N/A	N/A
C-BAND, FPS-16	15	SNFC	33.24771	240,47935	732,1500	335.	6263.
HEODOLITE	16	THE15	34,89239	241.99087	2696.6400	N/A	N/A
C-BAND, ALCOR	20	KMRC	9.39870	167.48199	86.0200	N/A	N/A

Table I. STS-14 station locations and refraction data.

EPOCH: 9/15/84 $12^{\text{h}}59^{\text{m}}0^{\text{S}}$ (46740^S) GMT

DATA TYPES:

COMMENTS:

S-band, 2 radars (GWMS, GDSS) C-band, 8 radars (KMRC, PTPC, VDBC, VDSC, SNFC, FRCC, EAFC) Cine-theodolite, 5 cameras (THEO1, THEO5, THEO7, THEO9, THE15)

5° Elevation constraint on C, S-band; No constraint on theodolite Excluded C-band Hawaii pass (KPTC) because of sparse, low elevation coverage Excluded noisy Range, Azimuth data during first half of Edwards pass (EAFC) Processed low rate (1/10s) S-band Range, X, Y-angle data from Guam (GWMS) received via JSC

Final Solution, BT14N02 ⁽²⁾	24077.667	-1.2893269	59.768329	668971.83	1.6843213	139.81285	57.381717	30.025645	-2.2729920	-0.118	1.344
BT14N01 (1)	24081.1	-1.279	59.769	664647.	1.679	139.809	57.379	30.018	-2.274	-0.943	5.044
JSC/TRW	24078.9	-1.287	59.770	668511.	1.684	139.812	57.338	30.001	-2.270	1	:
Initial Estimate, Nav	24079.0	-1.283	59.771	668949.	1.690	139.823	57.354) see	29.971 Appendix	-2.259 A	1 1	:
PARAMETER	V _R , fps	γ, deg	Ψ, deg	h_{η} , ft	Φ_{D} , deg	λ , deg	ψ, deg	θ , deg	φ, deg	n M	: <u>≯</u>

 $\overline{(1)}$ state only

Table II. STS-14 solution and comparisons.

⁽²⁾ state and accelerometer scale factors $\{\Delta SF_X, \Delta SF_Z \text{ (ppm)} = +5, +107, +18\}$

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WEIGHTED STAND, DEV.	.88834569E+00 .64368572E+00 .74234760E+00 .57632076E+00	.35267177E+00 .35267177E+00 .37395697E+00 .37395697E+00 .86384945E+00 .86384945E+00 .94308983E+00 .74356317E+00 .29134911E+00 .29134911E+00 .29134911E+01 .1956361E+01 .1956361E+01 .15286748E+01 .15286748E+01 .76239158E+00 .88627442E+00 .88627442E+00 .95112567E+00 .95112567E+00 .43224809E+00 .43224809E+00	.43880105E+00 .96623623E+00 .13436151E+01
STANDARD STAND. DEV.	.71552286E+01 .28947674E-01 .87875840E-02 .17672696E+02	.60931560E-02 .29739719E+02 .66322335E-02 .57156369E-02 .24362090E+02 .98989856E-02 .14806272E-01 .42603031E-02 .16693075E-02 .30601311E-02 .38553735E-02 .38553735E-02 .32401791E+02 .22418304E-01 .19520079E+02 .23594846E-01 .14752013E-01 .43681820E-02 .71210941E+01 .88238771E+00 .83422168E-02 .50779784E-02 .71210941E+01 .88238771E+00 .83422168E-02 .71210941E+01	.50282897E-02 .11072252E-01 WGT. STD. DEV. =
AVERAGE RESIDUAL	.55575846E+00 48143908E-01 13743056E-01	3986499E+039886439E+039886439E+039886439E+039886439E+039886439E+039886439E+039884E+039884E+039886439E+039886439E+03988649E+039886639E+0398E+039865E+039865E+039865E+039865E+039865E+039865E+0398355356E+03986423550E+039864235E+039986423E+03986422E+03986422E+03986422E+03986422E+03986422E+03986422E+03986422E+03986422E+0398642E+03986422E+03986442E+03986442E+03986442E+03986442E+03986444444444444444444444444444444444444	32766068E-02 .10150843E-01 =11837522E+00
AVERAGE WEIGHT, RES.	.11544246E-01 14001501E+01 11561571E+01 72710932E+00	2479309 247506295 27506295 27506295 27506295 27864525 27864525 27864525 27864525 27864525 27864525 27864525 278647333 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 277142965 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 27866605 278605 2786605 2786605 2786605 2786605 2786605 2786605 278605 2786605 2786605 2786605 2786605 2786605 2786605 2786605	28593788E+00 .88582814E+00 5783 WGT. MEAN
OBSERVATIONS ACCEPTED	0F 0F 0F	78800000000000000000000000000000000000	OF OF CS
OBSERVATION IE TYPE		AZIMUTH ELEVATION RANGE AZIMUTH ELEVATION AZIMUTH ELEVATION AZIMUTH ELEVATION AZIMUTH AZIMUTH ELEVATION AZIMUTH ELEVATION RANGE AZIMUTH ELEVATION RANGE AZIMUTH ELEVATION RANGE AZIMUTH ELEVATION RANGE AZIMUTH ELEVATION RANGE	KMRC AZIMUTH KMRC ELEVATION WEIGHTED FIT STATIS
STATION NO. NAME			20 20 TOTA L

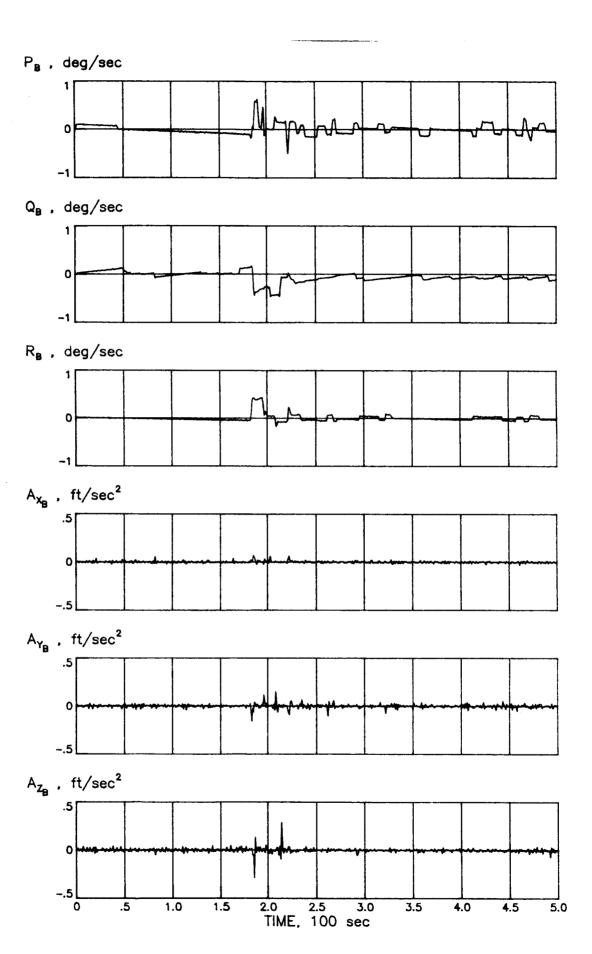


Figure I-1. STS-14 Dynamic data , IMU 2

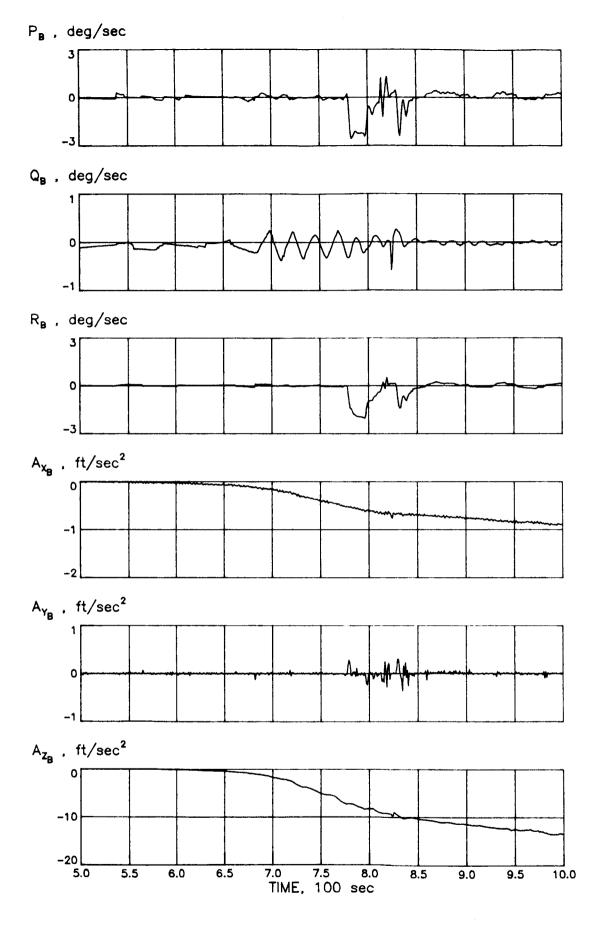


Figure I-1. (continued)

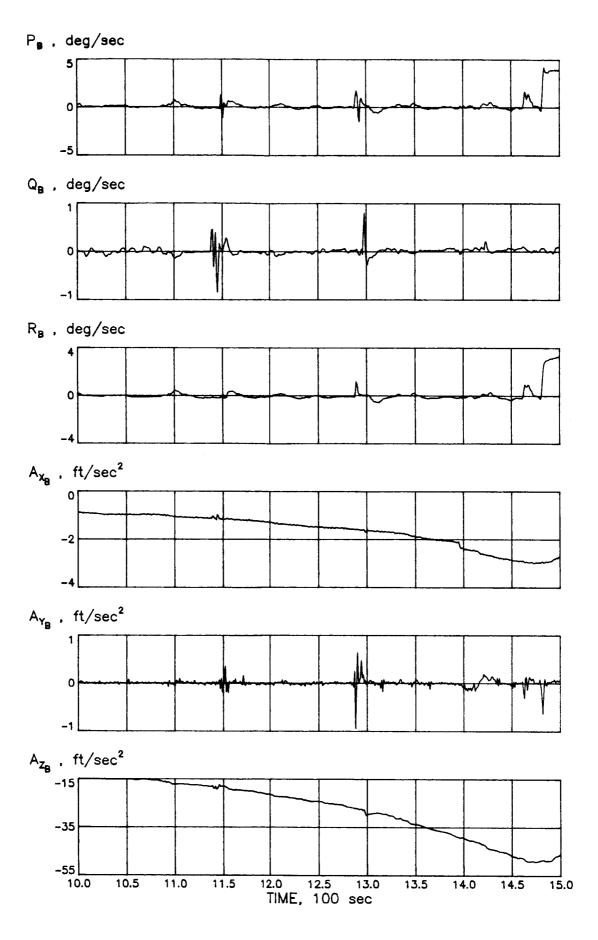
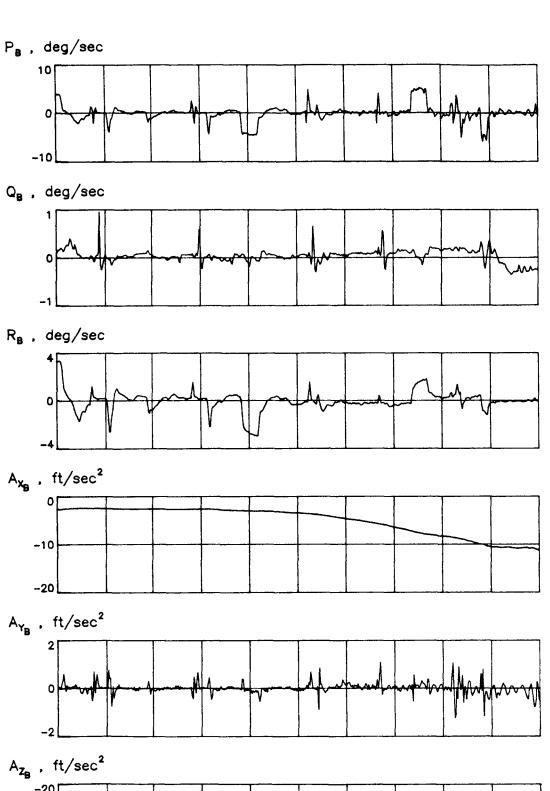


Figure I-1. (continued)



A_{Z_B}, ft/sec

-20
-40
-60
15.0 15.5 16.0 16.5 17.0 17.5 18.0 18.5 19.0 19.5 20.0 TIME, 100 sec

Figure I-1. (continued)

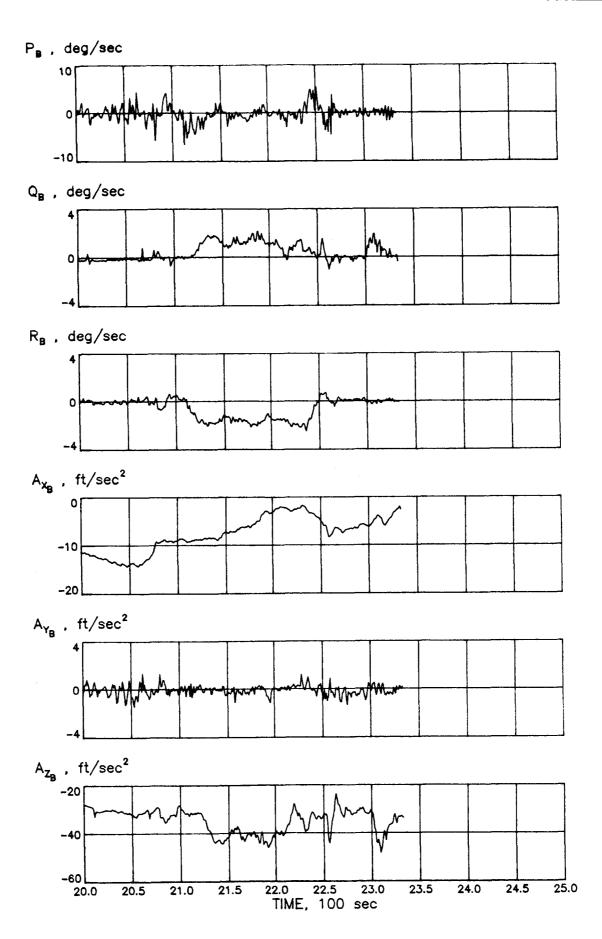


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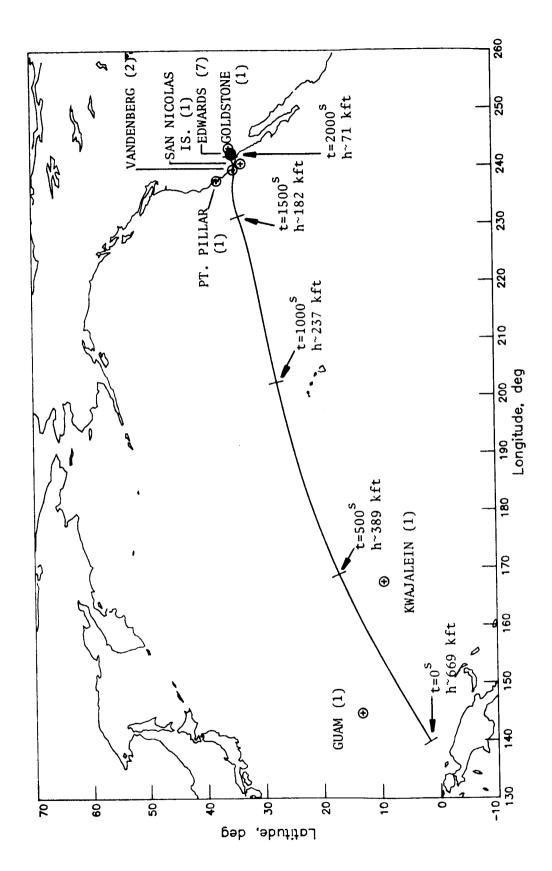
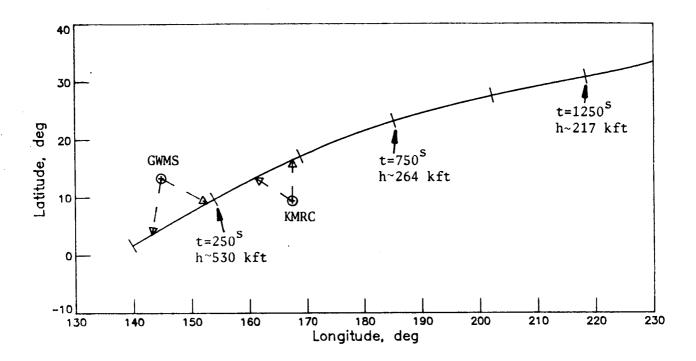
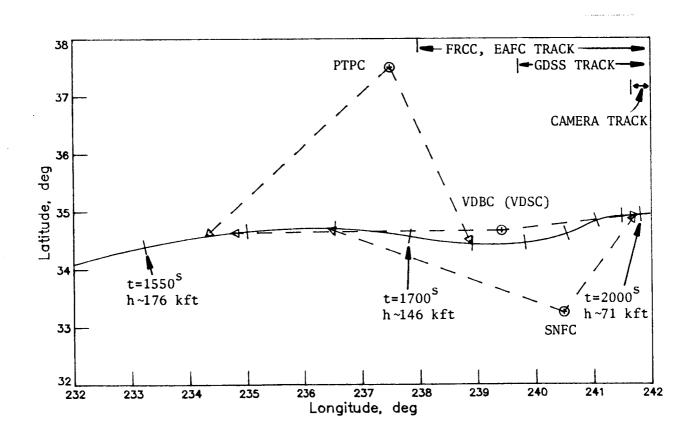


Figure I-2. STS-14 ground track from epoch to touchdown.



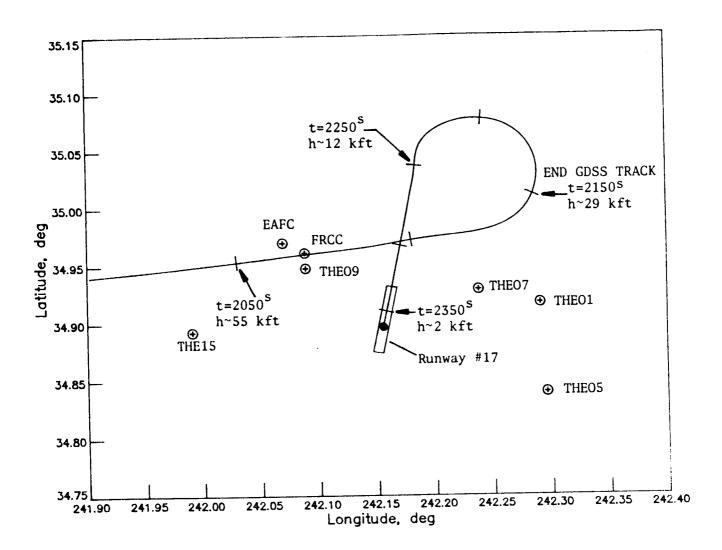
(a) Entry to California C-band acquisition.



(b) California C-band acquisition to final approach.

Figure I-3. Detailed tracking coverage for STS-14.

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(c) Final approach and landing

Figure I-3. (concluded).

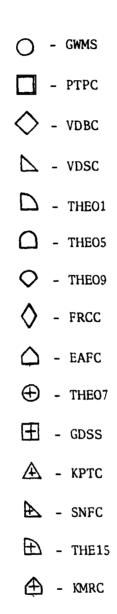


Figure I-4. Key for following three composite residual plots.

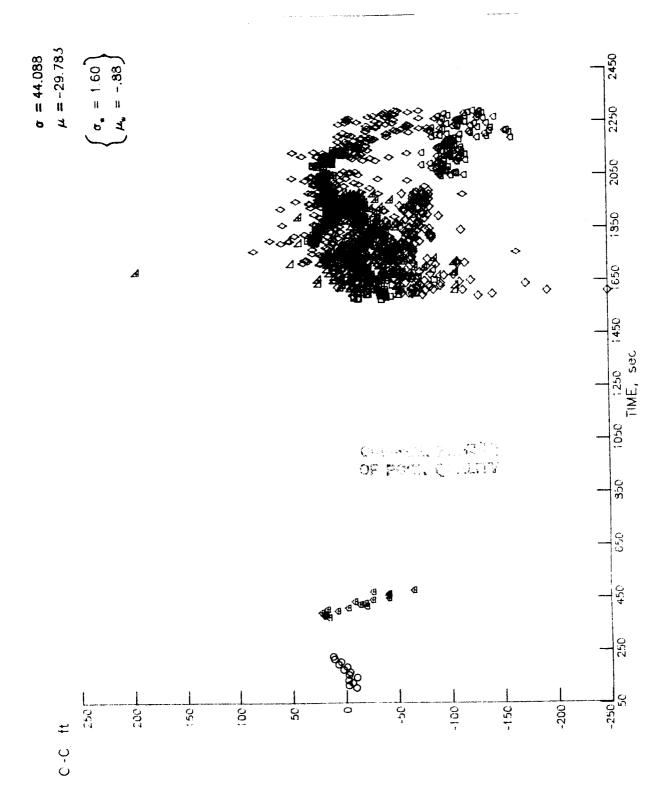


Figure I-5. STS-14 (41-D) composite range residuals.

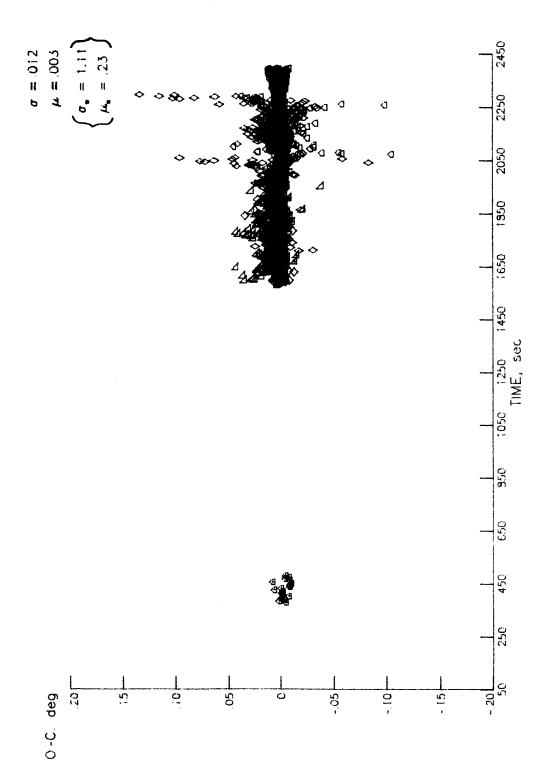


Figure 1-6. STS-14 (41-D) composite azimuth residuals.

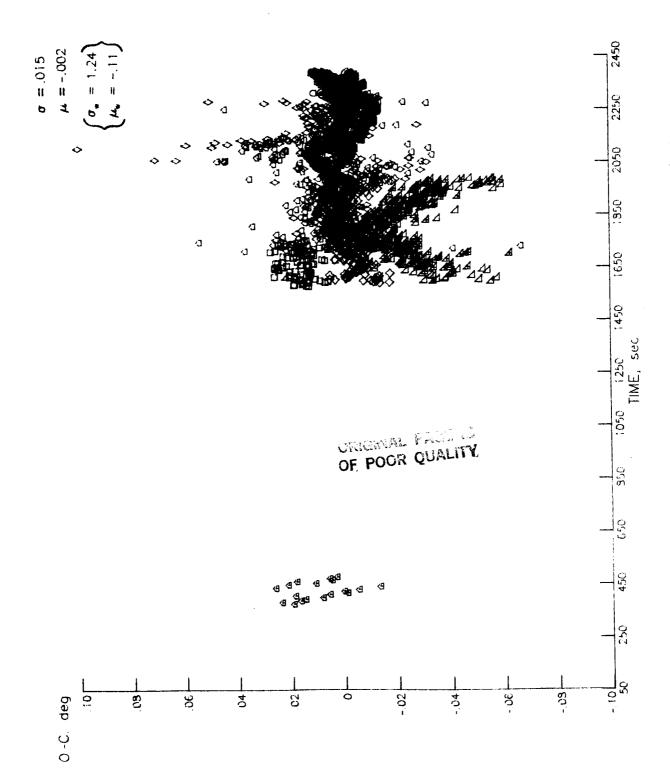


Figure I-7. STS-14 (41-D) composite elevation residuals.

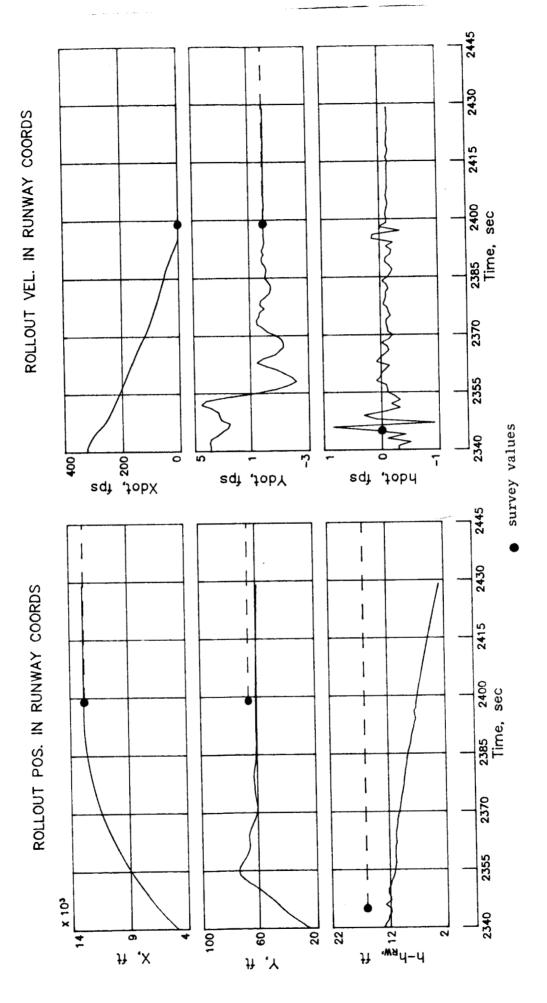


Figure I-8. Rollout position and velocity plots for STS-14.

II. Extended BET

This section presents comparisons of the available atmospheric source data which can be utilized with the inertial BET (BT14N02) for Extended BET development. These comparisons permit selection of a "best" atmosphere for the necessary air relative computations. Over the uppermost altitudes the selection process is somewhat arbitrary and involves comparisons of the two remote sources (LAIRS and NOAA (when available)) as well as the Air Force 1978 Reference Atmosphere Model. More recently, the Marshall Global Reference Atmosphere Model (GRAM) has also been incorporated. For the purposes of the LaRC analysis, the usual source of data is the LAIRS files which are developed by J. Mac Price of the Aerothermodynamics Branch. The available file for this flight is ST14MET/712662N. The equivalent NOAA "totem-pole" data were extracted from the JSC/TRW BET. Density (normalized to the 1976 Standard) and temperature comparisons based on these two remote sources as well as the previously mentioned models are shown as Figures II-1 and II-2, respectively. Differences between the two remote sources are exemplified by the shading thereon. Also shown are the derived quantities based on the measured normal acceleration and the predicted normal force coefficient, C_{Np} . It is noted, as was the case for the other September entry (STS-8), that the GRAM model is too dense above $h\sim240$ kft. Other than this obvious disparity, the other three sources would appear plausible. For the purposes herein, the LAIRS data were adopted. Figures II-3, 4, and 5 show the actual LAIRS temperature, pressure, and density profiles.

LAIRS atmospheric wind components are presented versus altitude as Figure II-6. Above Mach 1 (h~50 kft) there exists virtually no mechanism to evaluate these winds. However, during subsonic flight alternate measurements are available. Figure II-7 shows jimsphere balloon measurements from three balloons spaced approximately 2^h apart. Figure II-8 shows data from two of these balloons with LAIRS data and two estimates. The two estimates are batch and deterministic filtering results using the Rockwell post-flight air data information derived using in situ pressure measurements from the Orbiter side probes. No real discrepancies are noted, at least in view of the accuracies of each source, and thus the LAIRS winds were adopted. The final figure, II-9, shows actual differences between the computed and measured value of the important air relative parameters;

angle-of-attack, side-slip angle, and true air speed. These differences, though non-trivial, are again within the accuracy of the evaluation/estimation process.



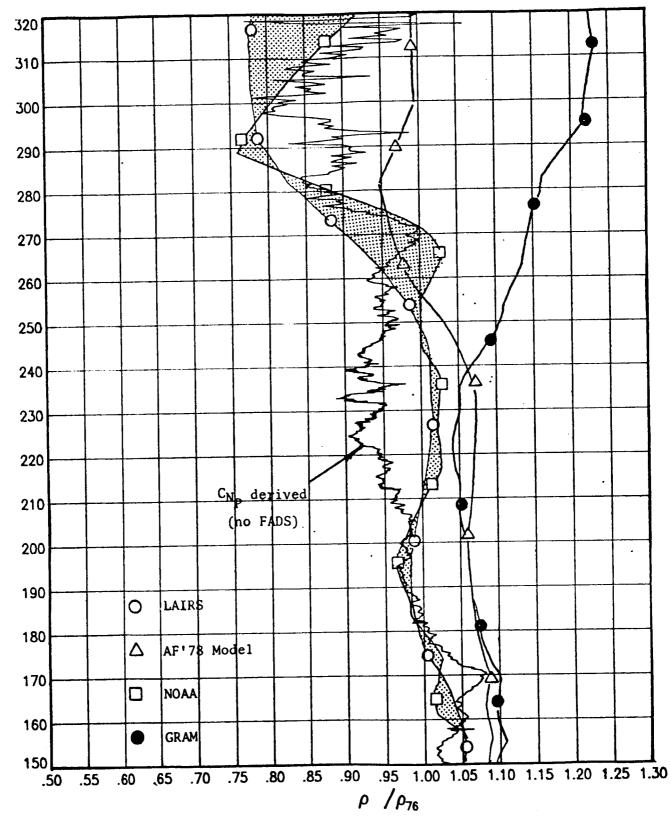


Figure II-1. Upper atmosphere density comparisons for STS-14 (41D).

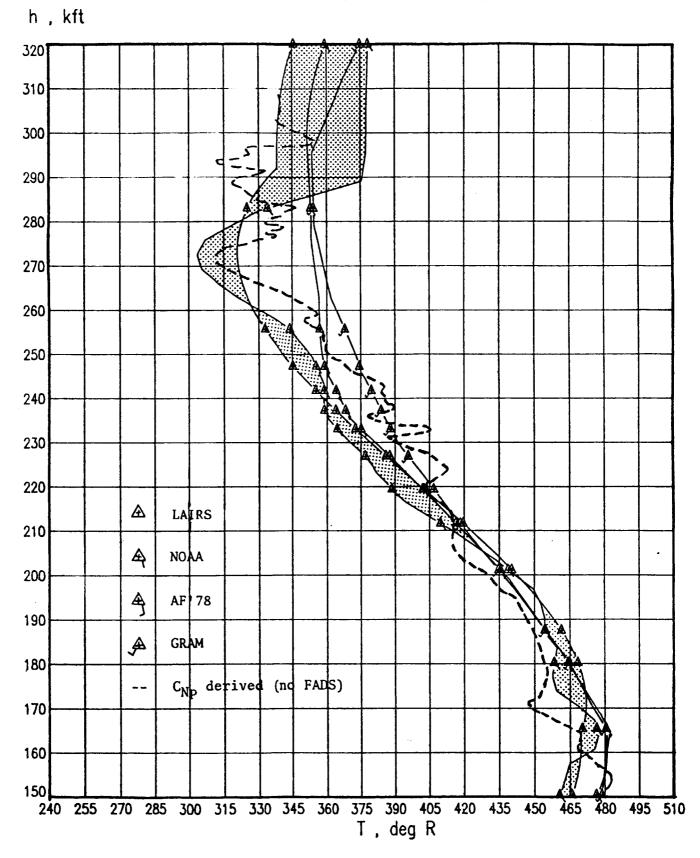


Figure II-2. Upper atmosphere temperature comparisons for STS-14 (41D).

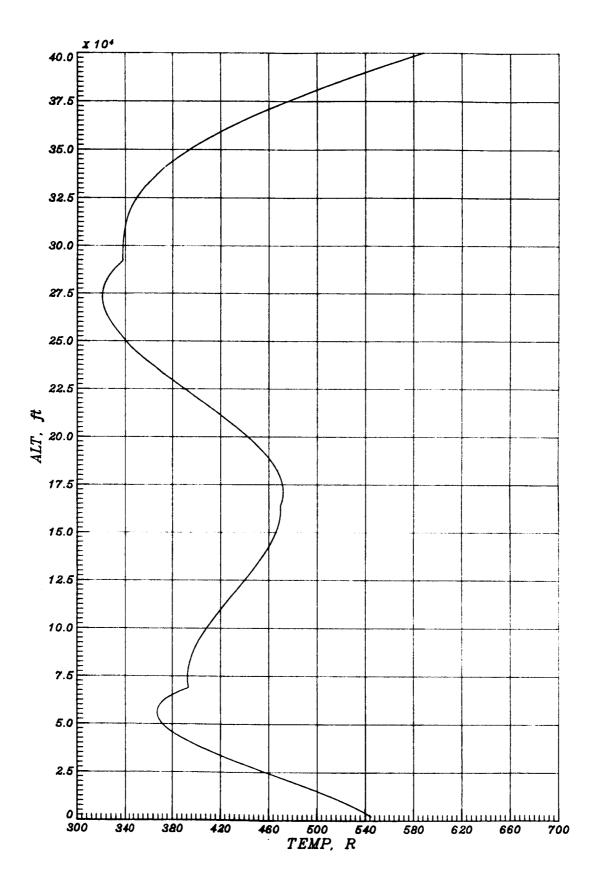


Figure II-3. Final STS-14 (41D) temperature profile.

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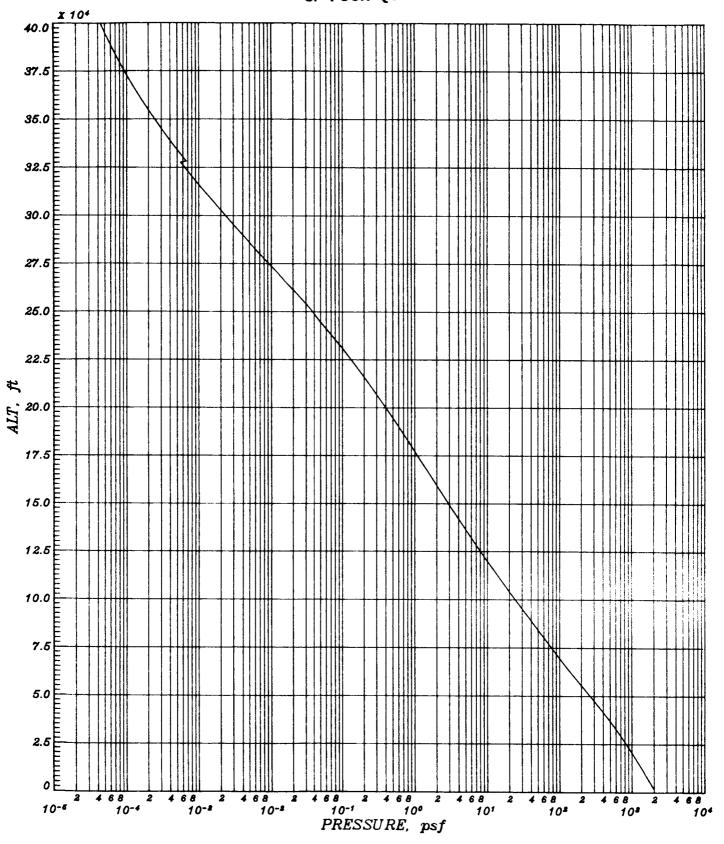


Figure II-4. Final STS-14 (41D) atmospheric pressure profile.

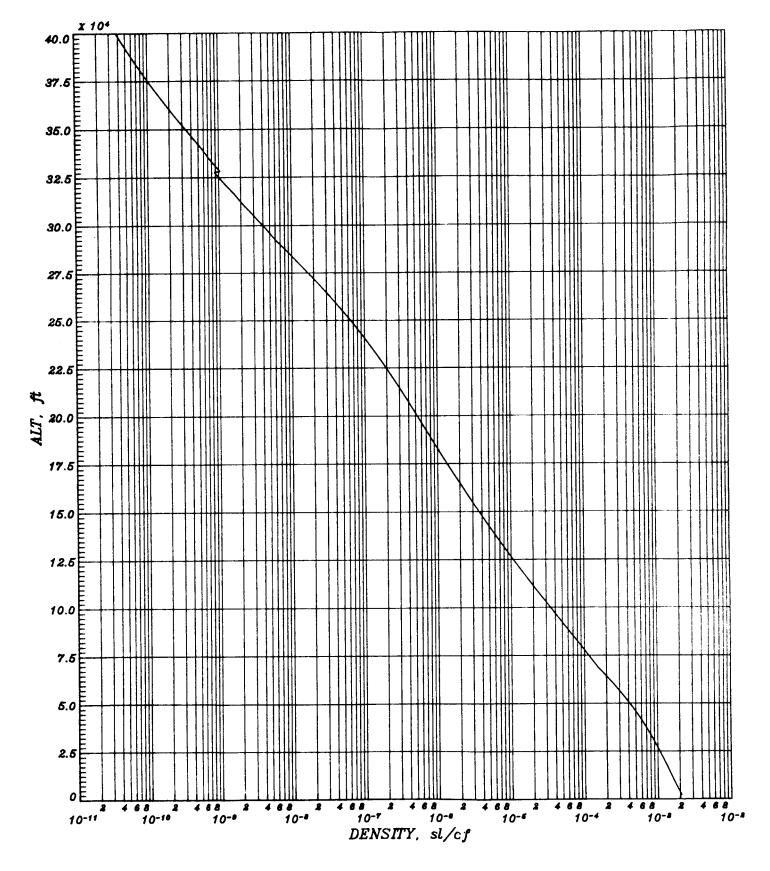


Figure II-5. Final STS-14 (41D) atmospheric density profile.

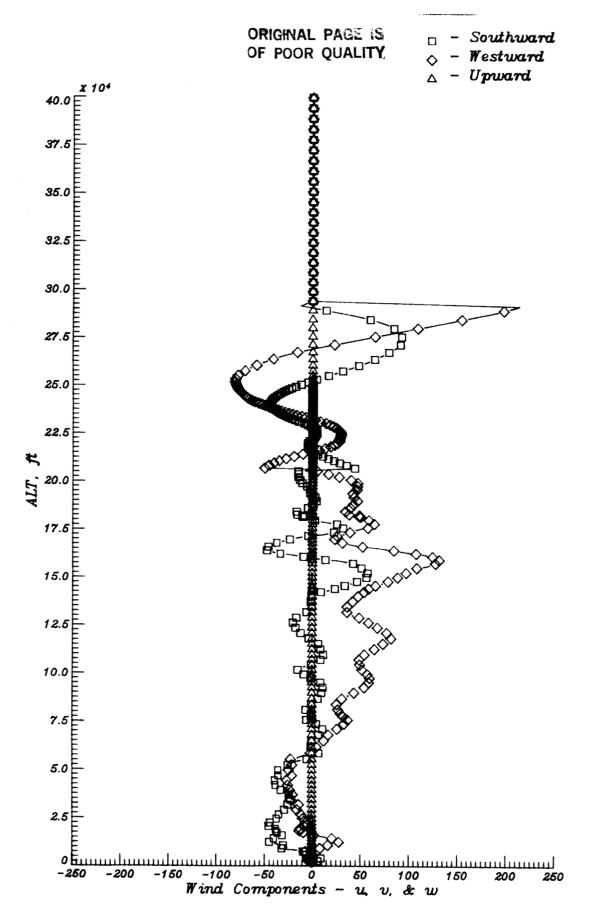
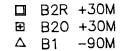
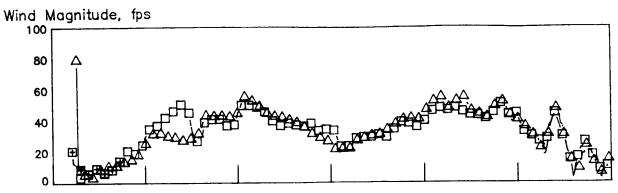
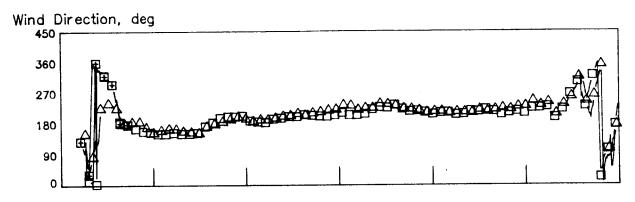
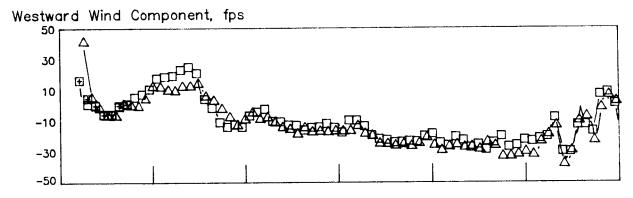


Figure II-6. Final STS-14 (41D) atmospheric wind profile.









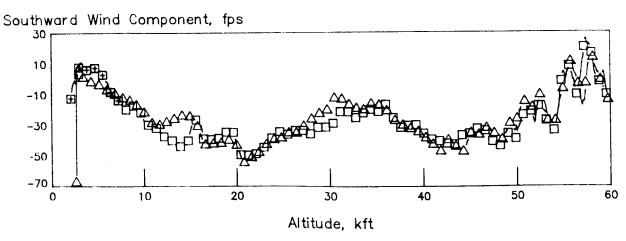
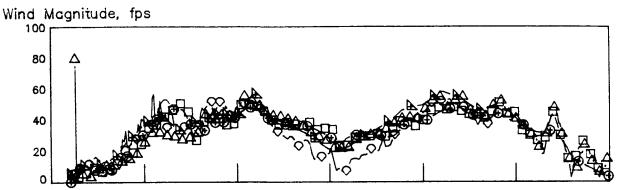
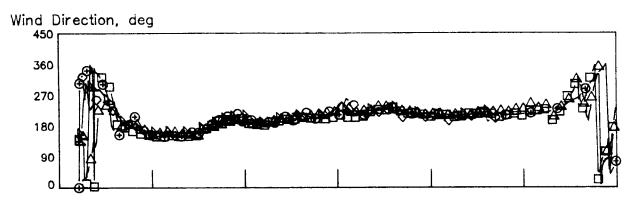


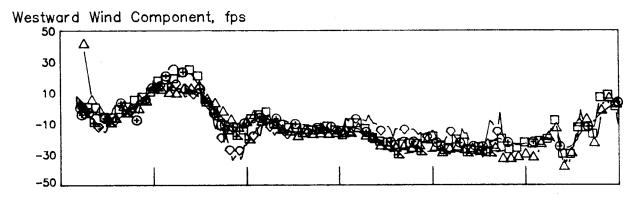
Fig. II-7. STS-14 Jimsphere Winds (2 Balloons)

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- ⊕ LAIRS□ B2R +30M△ B1 -90M
- DET-RCKWL BAT-RCKWL







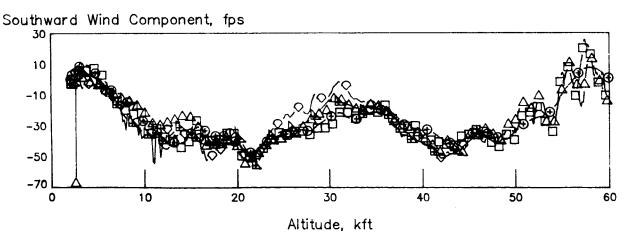


Fig. II-8. STS-14 Measured and Derived Winds

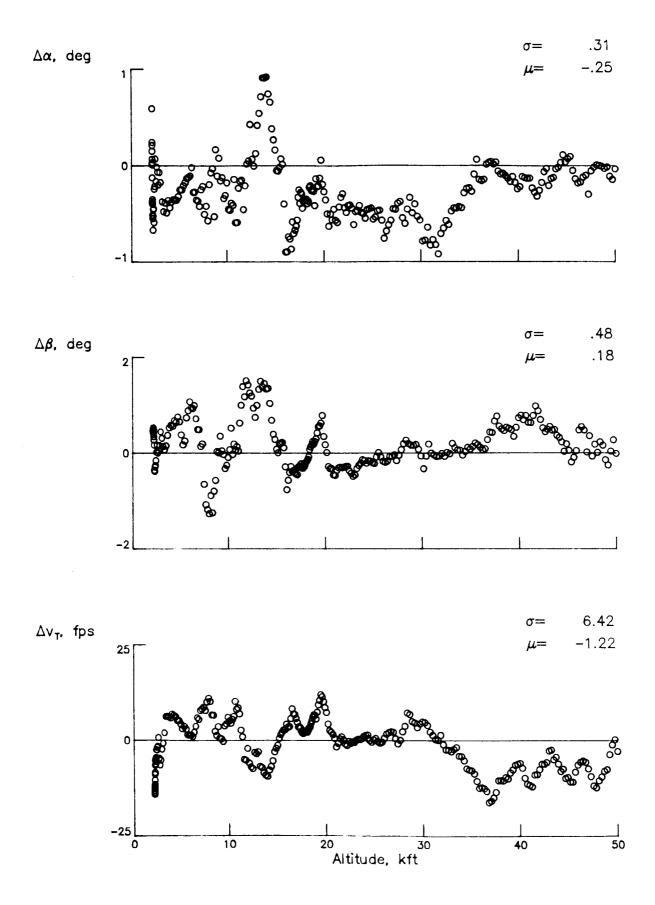


Fig. II-9. STS-14 ADP Differences, ST14ADS-ST14BET

III. Aerodynamic BET Discussion and Results

An AEROBET file was created based on the previously discussed Extended BET, ST14BET, utilizing the Operational Instrumentation recorded configuration information as well as the final spacecraft mass properties of Appendix A. Primary and back-up (duplicate) reels are NB1248 and NC0601, respectively. This section presents plots of some of the relevant parameters from the AEROBET, to include aerodynamic performance comparisons. Plots versus Mach No. are presented as semilog plots and the shaded bands thereon are based on the previous eleven flights.

Altitude versus time is presented as Figure III-1. Altitude rate, dynamic pressure, and Mach No. are presented versus both time and altitude as Figures III-2 through III-4, respectively. \bar{V}_{∞} and Reynolds No. are plotted versus altitude in Figures III-5 and III-6. Air relative attitude angles versus Mach and altitude are next presented. The shading on Figure III-7 shows the range of α 's encountered on the previous flights.

Spacecraft dynamic measurements, i.e., body axis components derived from IMU2, are plotted versus Mach No. in Figure III-9. Control surface deflections (vs. Mach and altitude) and RCS firings vs. Mach complete the configuration plots, viz, Figures III-10, 11, and 12. Again, the plots of control deflections versus Mach (Figure III-10) show the range of controller configurations flown previously. Some additional data base evaluation opportunities can be seen, e.g., more upward (negative) elevon deflections in the hypersonic regime; more downward (positive) body flap for 1<M<3, and speed-brake deflections above Mach 3.

Performance comparisons, Figures III-13 through III-15, show that Discovery is, as expected, aerodynamically similar to her two sister ships. Presented as Figures III-13 and III-14 are force (C_L , C_D , C_N , C_A), moment (C_m) and performance (L/D) comparisons. These data are with respect to the 65 percent reference c.g. commensurate with the Orbiter data base. The shaded region represents (statistically) the first eleven flight results. These ensemble results reflect a \pm 1 σ band about the mean difference ((flight-predicts)/flight) and compare,

except for rather narrow regions, with Discovery results. The final figure presented herein shows C_m comparisons at the flight c.g., to include flight, predicts, and expected variations. The hypersonic offset of ~0.028 due to real gas effects is suggested, which, for the most part, can be discounted by evoking "known" updates to the data base, i.e., the so-called Flight Assessment Deltas developed by project aerodynamicists.

^{*}Note boundary layer transition occurrence at the rather high Mach No. (~16), most visible in ΔC_A , $\Delta L/D$ plots.



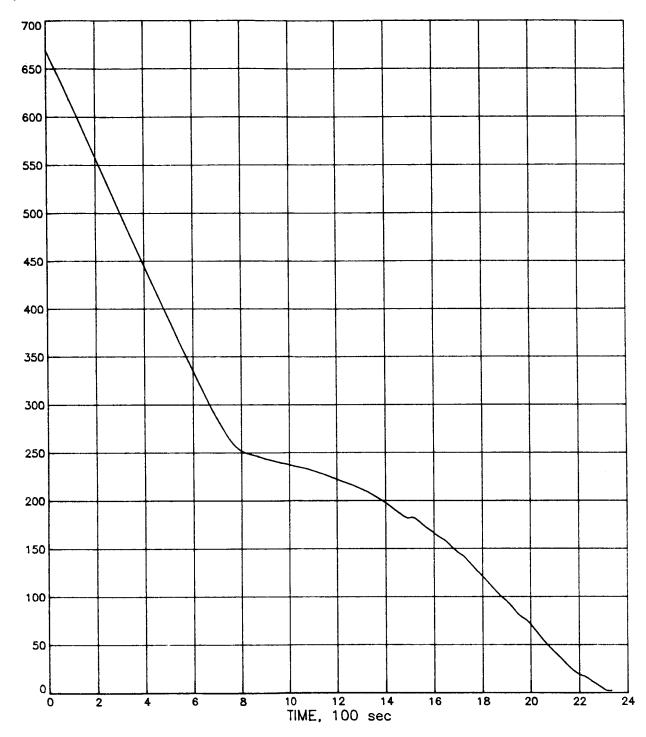
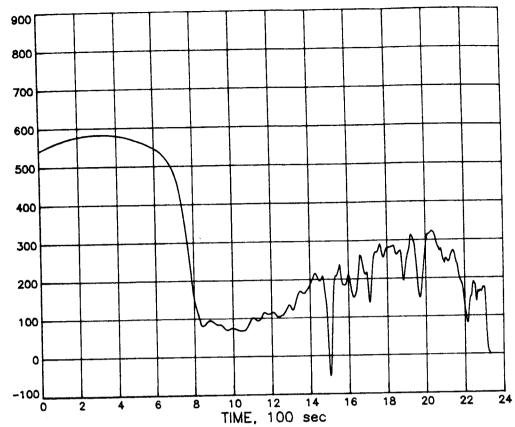


Figure III-1. STS-14 altitude time history







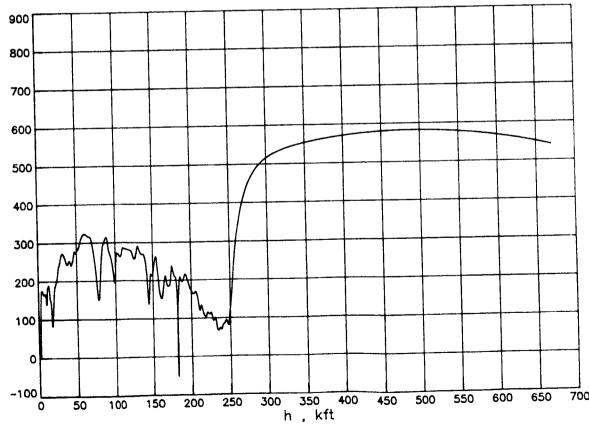
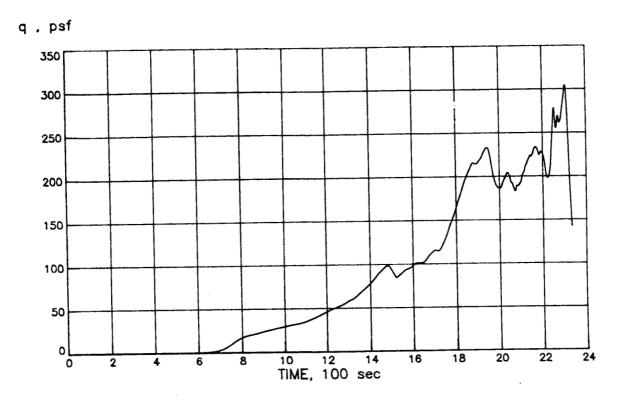


Figure III-2. STS-14 descent rate versus time and altitude (\dot{h} = -w) $^{-34-}$



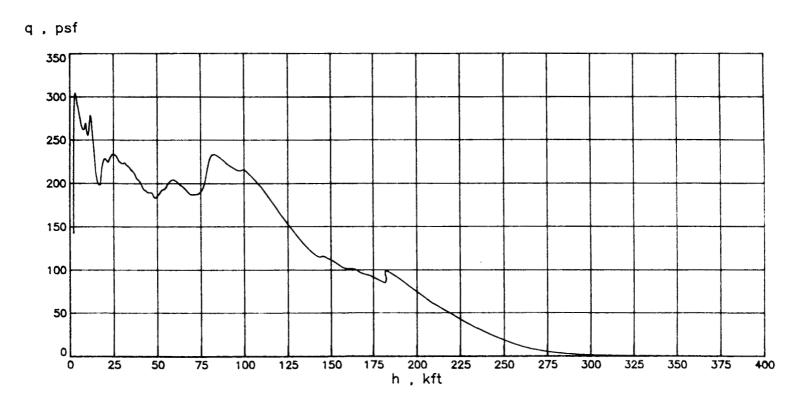
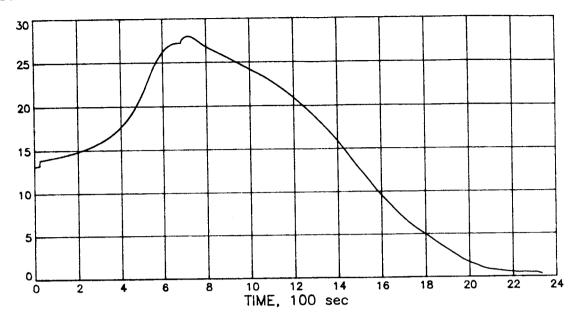


Figure III-3. STS-14 dynamic pressure vs. time and altitude





Mach

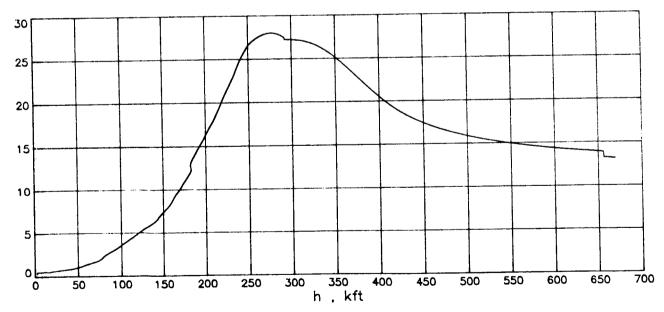


Figure III-4. STS-14 Mach number versus time and altitude

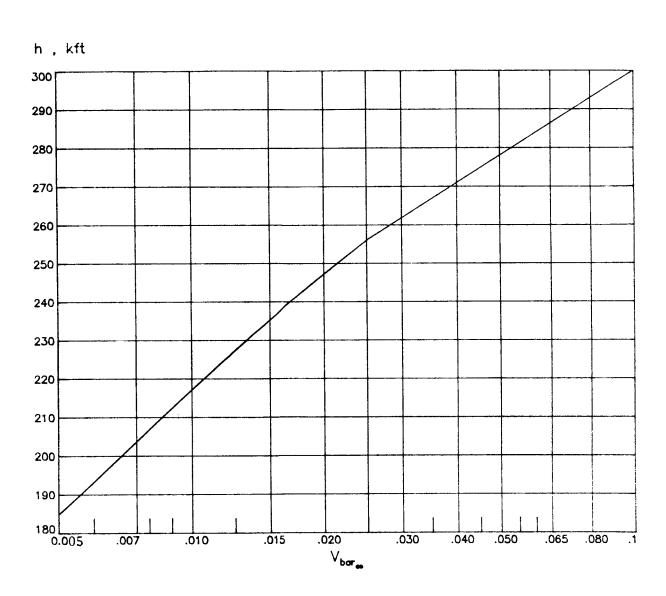


Figure III-5. STS-14 Vbar versus altitude

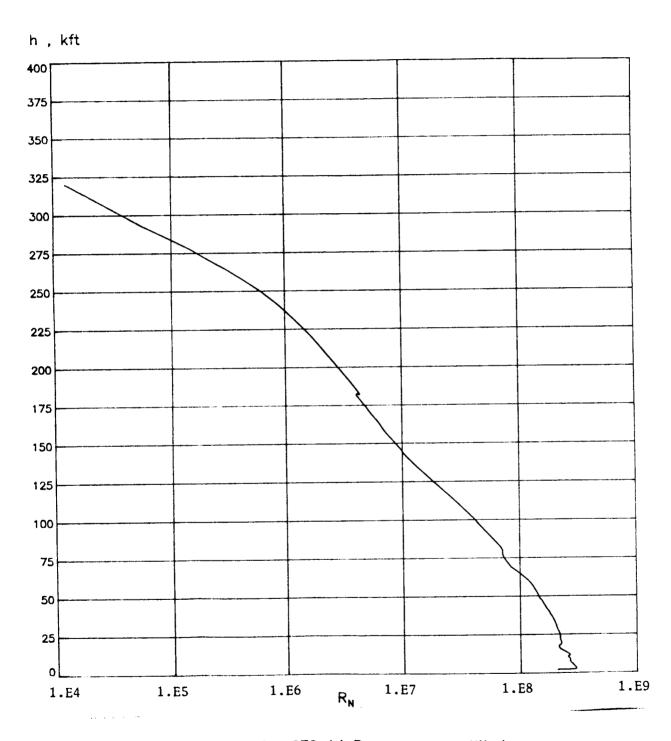


Figure III-6. STS-14 Rnum versus altitude

ORIGINAL PAGE IS OF POOR QUALITY α , deg 50 45 40 35 30 25 20 15 10 5 $\boldsymbol{\beta}$, deg σ , deg 90 45

Figure III-7. STS-14 α , β and σ vs. Mach

Mach

2.5 3.0

4.0

6.0

8.0 10.0

1.5

2.0

1.0

0

-45

-90 L .3

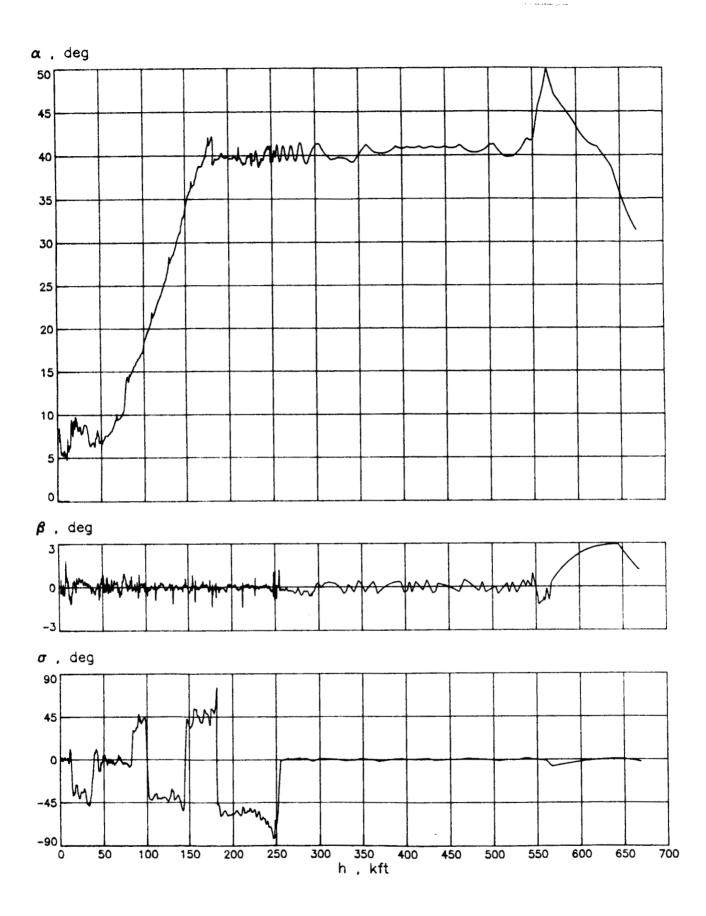


Figure III-8. STS-14 α , β and σ vs. h

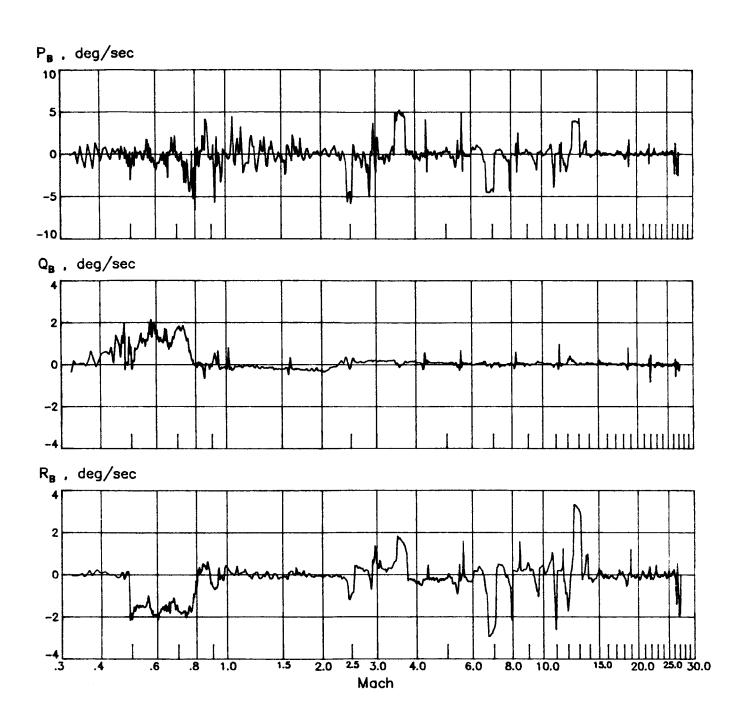


Figure III-9. STS-14 dynamic data vs. Mach

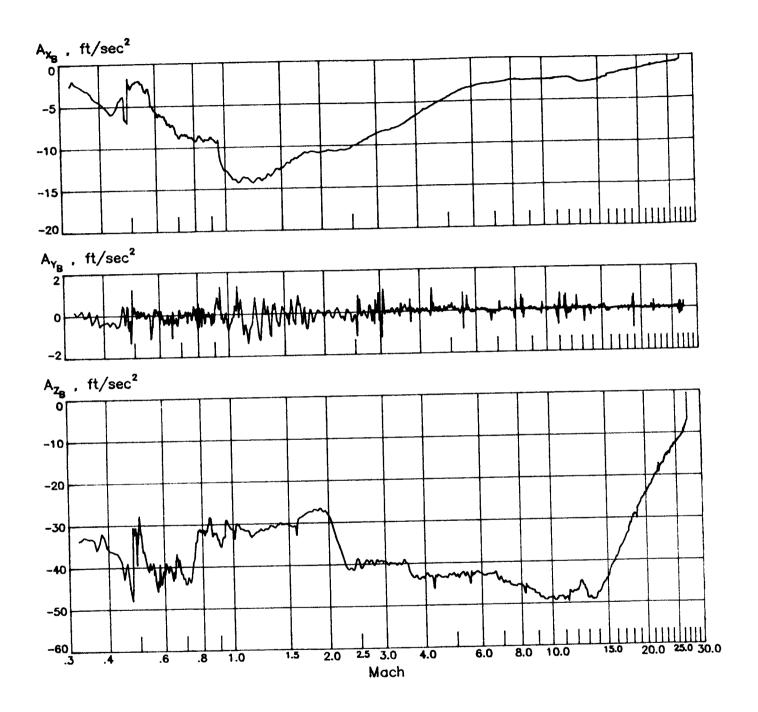


Figure III-9. (concluded)

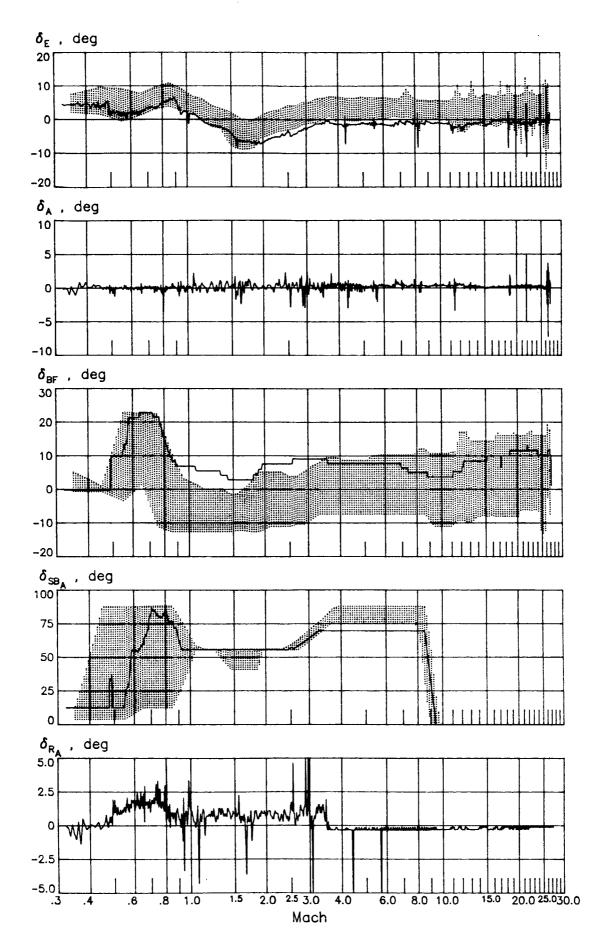


Figure III-10. STS-14 control surfaces vs. Mach

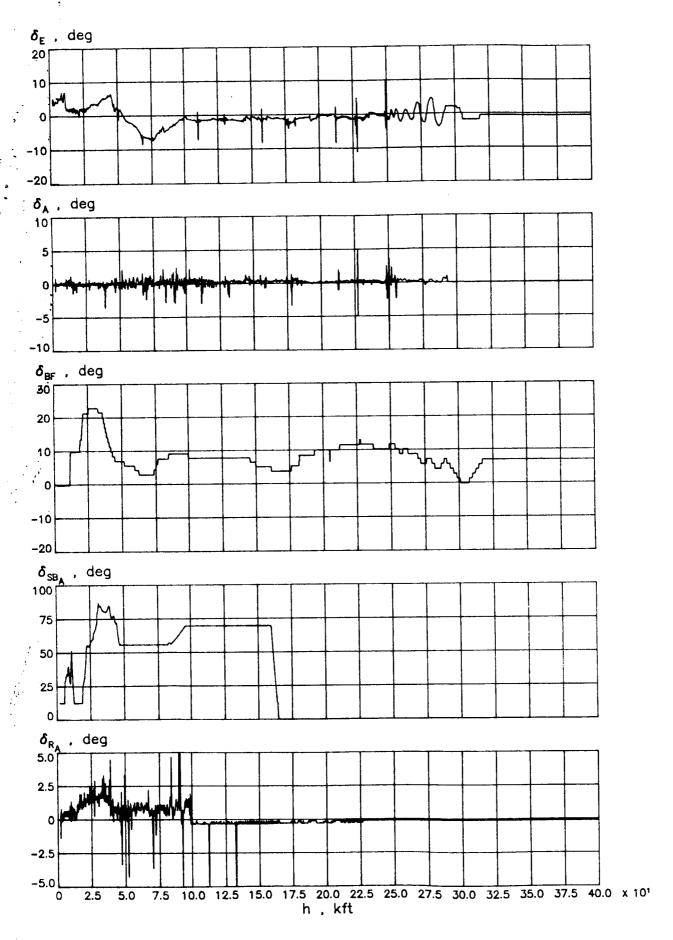


Figure III-11. STS-14 control surfaces vs. altitude

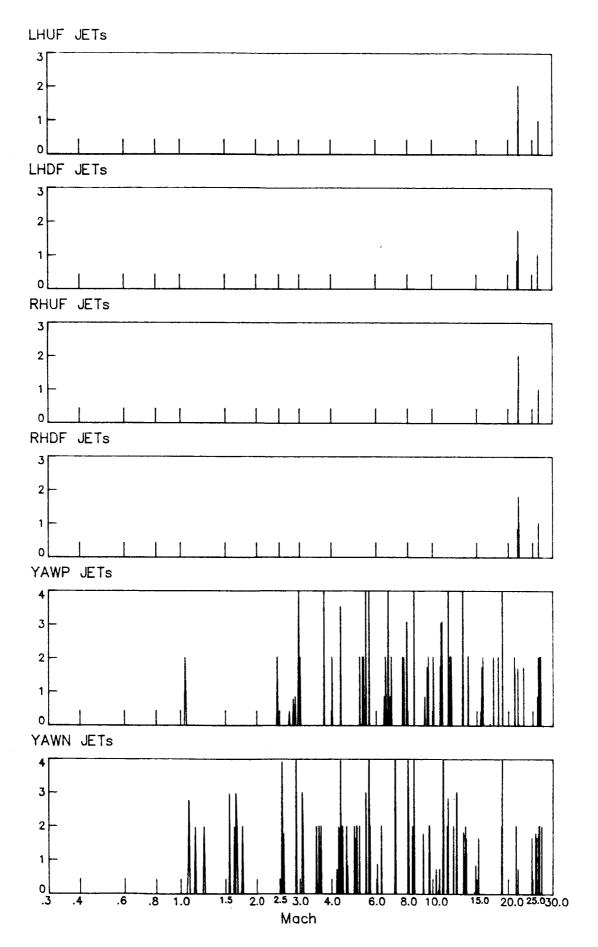


Figure III-12. STS-14 RCS firings vs. Mach

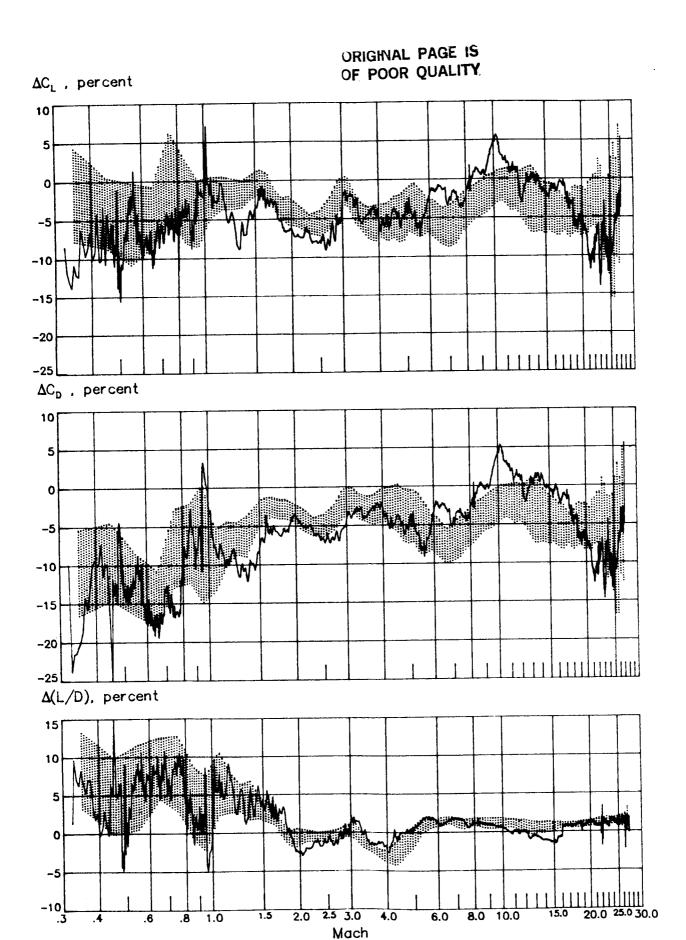


Figure III-13. STS-14 flight/data base differences vs. Mach

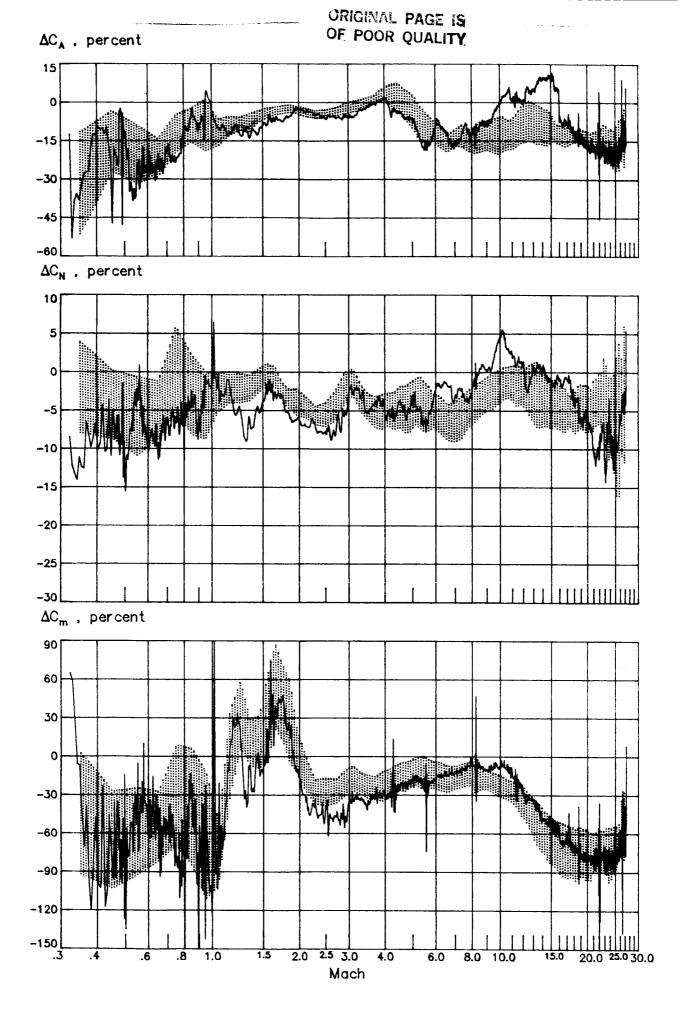


Figure III-14. STS-14 flight/data base differences vs. Mach -47-

C_m

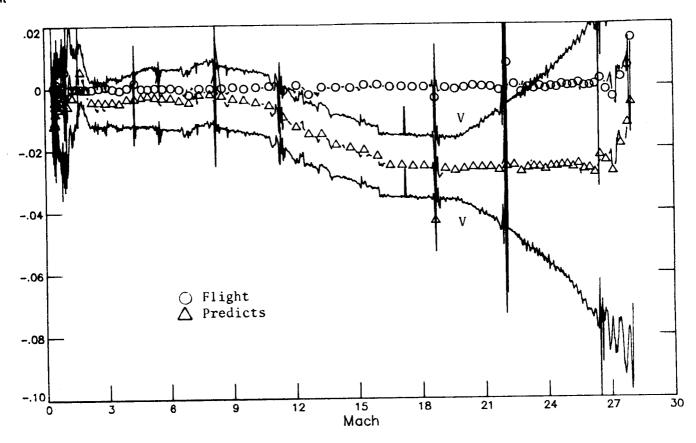


Figure III-15. STS-14 C_m comparisons vs. Mach (at the flight c.g.)

IV. MMLE Input File Generation (GTFILES)

MMLE input files were generated for STS-14 maneuver analyses. Maneuver activity during this flight is summarized as Table IV herein. GTFILEs were generated using the IMU2 data as well as the RGA1/AA1 data. ACIP data are not available on any of the Discovery flights. Files created are on nine-track reels NW0766 (based on IMU2) and NR0101 (replacing IMU2 measurements with the merged, rectified, RGA1/AA1 data). The extent of bias removal for rectification of these latter data is shown as Figures IV-1. Here, 100 second sub-interval biases (relative to the more accurate IMU2 data) were computed. These plots start at t = 480 seconds from epoch (h~400 kft), i.e., well above appreciable signal in the accelerometry. Annotated on each sub-figure are the ensemble mean (μ_{avg}) over the entire time span as well as an estimate in the variation (1 σ) of the mean difference over the arc.

STS-14 PTIs

LATERAL/DIRECTIONAL

PTI#	DURATION (secs)	START TIME	TIME FROM EPOCH (secs)	STOP TIME	TIME FROM EPOCH (secs)
1	14	249:13:12:31.0	811	13:12:45.0	825
2	8.5	13:18:07.5	1147.5	13:18:16.0	1156
3	12	13:20:27.0	1287	13:20:39.0	1299
4	9	13:24:34.0	1534	13:24:43.0	1543
5	9	13:26:20.0	1640	13:26:29.0	1649
6	8.5	13:28:16.5	1756.5	13:28:25.0	1765
7	8	13:29:29.0	1829	13:29:37.0	1837
8	15	13:30:48.0	1908	13:31:03.0	1923
9	7.5	13:32:21.0	2001	13:32:28.5	2008.5
10	11.5	13:33:12.5	2052.5	13:33:24.0	2064
11	8	13:33:37.0	2077	13:33:45.0	2085

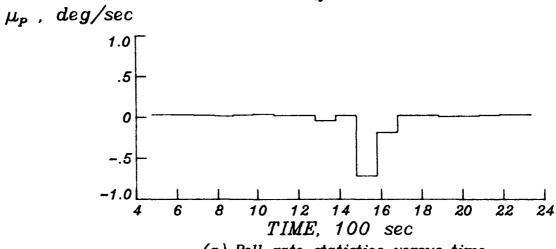
LONGITUDINAL

PTI#	DURATION (secs)	START TIME	TIME FROM EPOCH (secs)	STOP TIME	TIME FROM EPOCH (secs)
1	9.5	249:13:12:42.0	822	13:12:51.5	831.5
2	17.5	13:17:57.5	1137.5	13:18:15.0	1155
3	6	13:20:36.0	1296	13:20:42.0	1302
4	9	13:24:42.0	1542	13:24:51.0	1551
5	5	13:26:28.0	1648	13:26:33.0	1653
6	6	13:28:24.0	1764	13:28:30.0	1770
7	6	13:29:37.0	1837	13:29:43.0	1843
8	4	13:32:29.0	2009	13:32:33.0	2013
9	5	13:33:25.0	2065	13:33:30.0	2070
10	3	13:33:44.0	2084	13:33:47.0	2087

Table IV Aerodynamic extraction maneuvers for STS-14.

$$\sigma_{\mu} = .17534$$

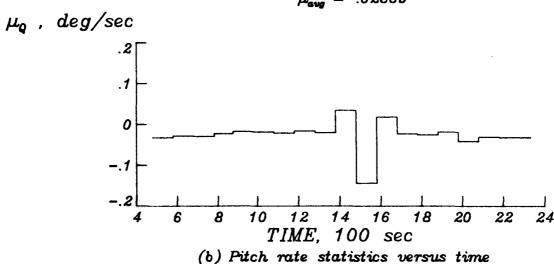
$$\mu_{\text{avg}} = -.02880$$



(a) Roll rate statistics versus time

$$\sigma_{\mu} = .03413$$

$$\mu_{avg} = -.02569$$



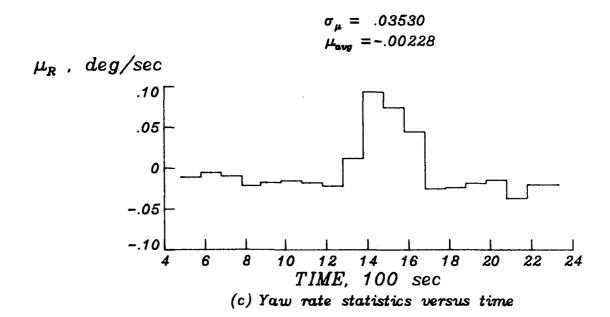
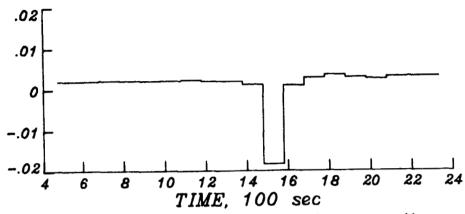


Figure IV-1. Dynamic data comparisons for STS-14.

$$\sigma_{\mu} = .00482$$

$$\mu_{\text{avg}} = .00108$$

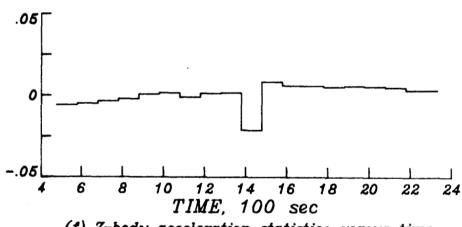




(e) Y-body acceleration statistics versus time

$$\sigma_{\mu} = .00673$$
 $\mu_{mag} = .00061$

$\mu_{\mathbf{A_z'}}$ g's



(f) Z-body acceleration statistics versus time

Figure IV-1. (Concluded).

 $\label{eq:APPENDIX} \mbox{ A}$ Spacecraft and Physical Constants

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+++++IMU NBR 1 ATTITUDE II	NFORMATION++++	
INFRTIAL (FE50) TO ROTA	ATING (FTOD)	
99987753F+00	.15289406E-01	.33417625E-02
15289286E-01	99988311E+00	.61723721E-04
.33423156F-02	.10623000E-04	.99999441E+00
ROTATING (ETOD) TO N-E	-0	
.22382694E-01	18899569E-01	•99957082E+00
64515346F+00	76405302F+00	0.
•76372510F+00	-,64487657F+00	-,29294687F-01
NAV BASE TO S/C BODY		
•98286611F+00	.11081625E-03	18432090E+00
35601724E-03	.99999910F+00	12972003E-02
•18432059F+00	.13340596E-02	.98286526E+00
NAV BASE TO OUTER ROLL		
•9999683F+00	272747685-02	11707061E-02
•22274753E-02	.99999752E+ 0 0	26077272E-05
•11707090F-02	0.	•9999932E+00
PLATFORM TO DUTER ROLL		
.76891678E-01	.42385172F+00	90246135F+00
80436742E+00	50846260E+00	30733917E+00
58913481E+00	•74954255E+00	•30183682E+00
INFRTIAL (FF50) TO PLA	TFORM	
.52808990E-01	75718081E+00	.65106714E+00
26077759E+00	.61889690F+00	•74091947F+00
96395344F+00	20891094F+00	16477245E+00
S/C BODY TO N-F-D		
.46823397F+00	85131582F+00	.23668481E+00
•72942144F+00	•52358210F+00	.44027907E+00
49869895E+00	33492648E-01	.86612795E+00

TABLE A-1

STS-14 IMU Attitude Matrices @ Epoch.

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+++++IMU NBR 2 ATTITUDE INFORMATION+++++

THERTIAL (FESO) TO POT	ATING (ETOD)	
99987753E+00	•15289406E-01	•33417625E-02
15289286E-01	99988311E+00	.61723721E-04
.33423156F-02	.10623000E-04	.99999441E+00
POTATING (ETOD) TO N-E-	- ը	
•22382694E-01	18899569E-01	•99957082E+00
64515346F+00	76405302F+00	0•
•76372510F+00	64487657E+00	29294687E-01
NAV RASE TO S/C BODY		
•98286611F+00	.11081625E-03	18432090E+00
35601724E-03	.99999910E+00	12972003F-02
.18432059F+00	•13340596F-02	.98286526E+00
NAV BASE TO OUTER POLL		
.99999707F+00	14653600E-02	19236980E-02
•14654087E-02	•99999892E+00	.23933827E-04
•19236609F-02	26752760E-04	•99999810E+00
PLATFORM TO DUTER ROLL		
21777010F+00	•71647936E+00	.66274643E+00
77116723F+00	54252570E+00	.33311575E+00
•59822788E+00	43854571F+00	.67067196E+00
INFRTIAL (FF50) TO PLA	TFORM	
77244341E+00	•14704973E+00	.61782485E+00
•56492066E+00	28538144F+00	•77422351F+00
•29016513E+00	•94706589E+00	•13736957E+00
S/C BODY TO N-F-D		
.46740550E+00	85189071E+00	•23625452E+00
•72898058F+00	•52258518F+00	.44214078E+00
50011856F+00	34439758F-01	.86527169E+00

+++++IMU NRP 3 ATTITUDE INFORMATION+++++

•		
INERTIAL (EE50) TO POTA	TING (FTOD)	
999877535+00	.15289406F-01	•33417625E-02
15289286E-01	99988311F+00	.61723721E-04
.33423156F-02	.10623000E-04	.99999441E+00
POTATING (ETOD) TO N-E-	-D	
•22382694F-01	18899569F-01	•99957082E+00
44515346E+00	76405302F+00	0.
.76372510F+00	64487657E+00	29294687E-01
NAV BASE TO S/C BODY		
.98286611F+00	.11081625F-03	18432090F+00
35601724F-03	.99999910E+00	12972003E-02
.18432059F+00	.13340596E-02	.98286526E+00
•		
NAV BASE TO OUTER POLL		
.9999950F+00	67501024E-03	•72914753F-03
.67503720F-03	•9999977E+00	36723830E-04
72912257E-03	.37216013E-04	•9999973F+00
• •		
PLATFORM TO OUTER ROLL		
.88834251F+00	39263663F+00	.23808409E+00
39817090F+00	91692831E+00	26493220E-01
.22870831E+00	71263116E-01	97088286E+00
INFRTIAL (EF50) TO PLAT	TFORM	
	.40278077E+00	.81939709E+00
61584227F+00		.57257527F+00
.67407888E+00	73815423F+00	.27312030E-01
S/C BODY TO N-F-D		
.46629774E+00	85275411E+00	.23532775E+00
.72987297E+00	•52117095F+00	.44233806E+00
49985169E+00	34507510F-01	.86542320E+00
* · · · · · · · · · · · · · · · · · · ·		

TABLE A-1 (Concluded).

Planet Parameters

Physical Model

Polar Radius: Equatorial Radius: Rotational Rate: 20,855,591.48 ft 20,925,741.47 ft .7292115147E-4 rad/sec

Gravity Model

Runway 17 Location:

Altitude: Geodetic Latitude:

Longitude:
Azimuth:

2090.ft (above ellipsoid)

34.930885 deg 242.163116 deg 190.072211 deg

Location of IMU relative to center-of-gravity in Body coordinates

(6-point table used for entry reconstruction)

TIME, sec	X_{B} , ft	Y_{B} , ft	Z_{B} , ft
0	56.1928	0.0250	-4.0417
480	56.1928	0.0250	-4.0417
1915	55.9761	0.0250	-4.1167
2314	55.9761	0.0250	-4.1167
2314.01	56.1094	0.0250	-4.3417
3000	56.1094	0.0250	-4.3417

Spacecraft aerodynamic reference parameters

 Reference Area
 2690 ft²

 Span
 78.057 ft

 Chord
 39.567 ft

Average Attitude Computations @ Epoch (46740 sec)

	IMU1	IMU2	IMU3	<u> </u>	<u>σ</u>
ψ(deg)	57.3026	57.3329	57.4265	57.3540	0.0646
θ (deg)	29.9140	30.0078	29.9902	29.9707	0.0499
φ(deg)	-2.2145	-2.2793	-2.2834	-2.2591	0.0386

TABLE A-2

Planet and Spacecraft Data Used for BT14N02, ST14BET, and AEROBET Generation

Weight and Center-of-Gravity (c.g.) Location

EVENT	TIME	WEIGHT	x_{CG}	Y_{CG}	z_{CG}
	(sec from epoch)	(1bs)	(inches in	Orbiter Struct	ural Reference)
EI	480	203530.5	1093.5	-0.3	373.5
М3	1915	202466.5	1090.9	-0.3	372.6
Landing	2333	202336.5	1092.5	-0.3	369.9

Moments and Products of Inertia

EVENT	IXX	I _{YY}	IZZ	IXY	IXZ	IYZ
EI	895931.5	6738859.2	7024474.3	13829.3	181084.5	-2078.6
М3	887861.6	6679180.0	6968767.1	14375.9	163649.0	-1920.3
Landing	917348.1	6700003.2	6964771.4	14469.1	157153.9	-1961.3

NOTES

EI values assumed at epoch

Mach 3 values held constant until gear deploy (t=2314), landed values adopted thereafter

APPENDIX B

Final residuals for STS-14 trajectory reconstruction

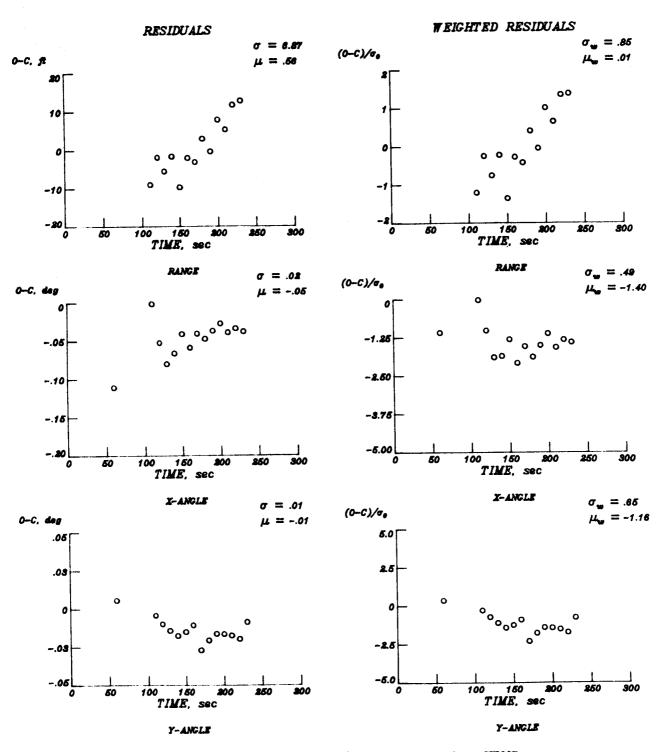


Fig. B-1. Smoothed residuals versus time for GWMS

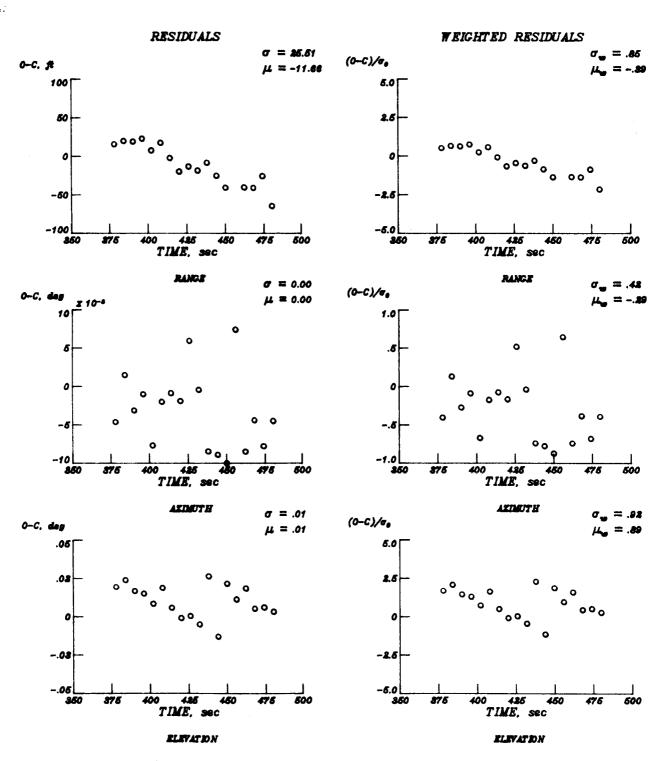


Fig. B-2. Smoothed residuals versus time for KMRC

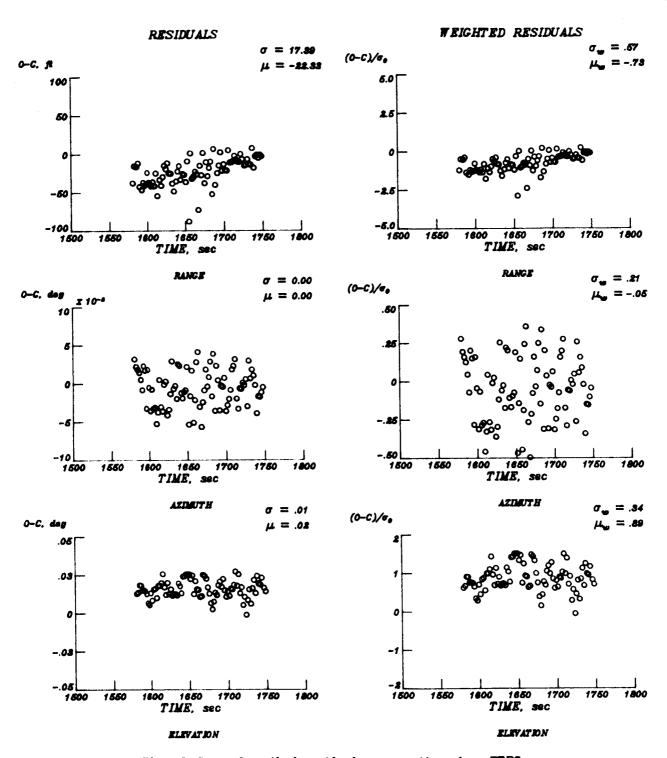


Fig. B-3. Smoothed residuals versus time for PTPC

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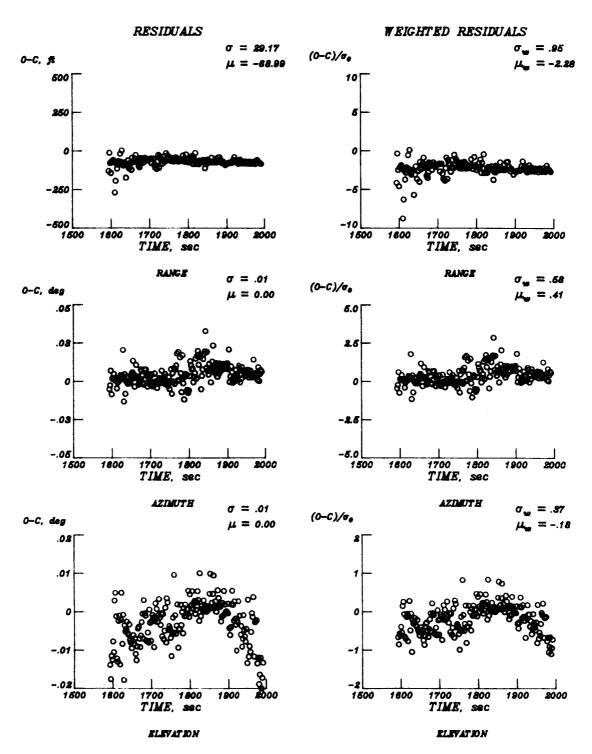


Fig. B-4. Smoothed residuals versus time for VDBC

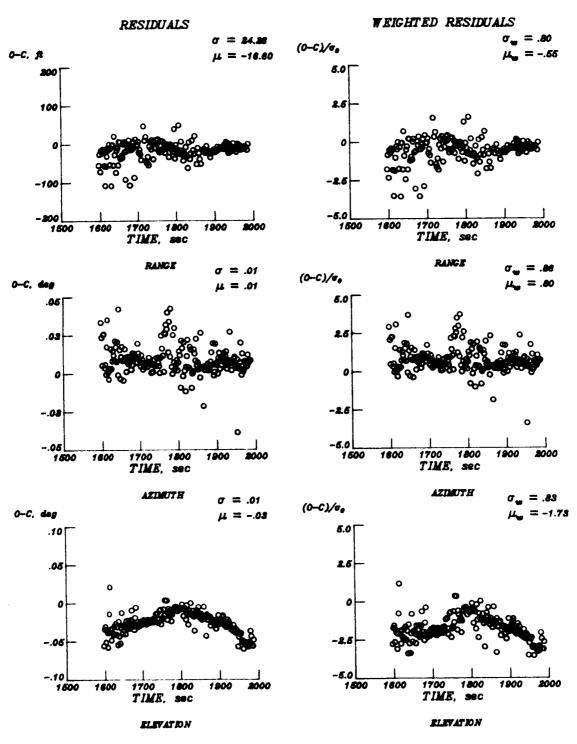


Fig. B-5. Smoothed residuals versus time for VDSC

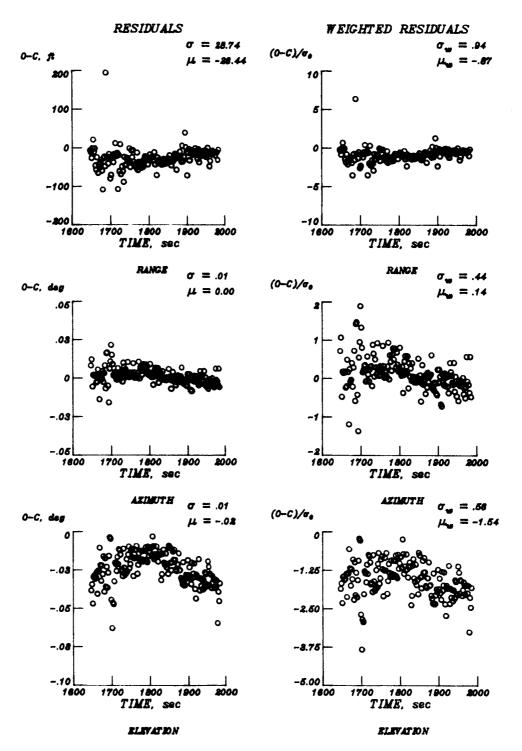


Fig. B-6. Smoothed residuals versus time for SNFC

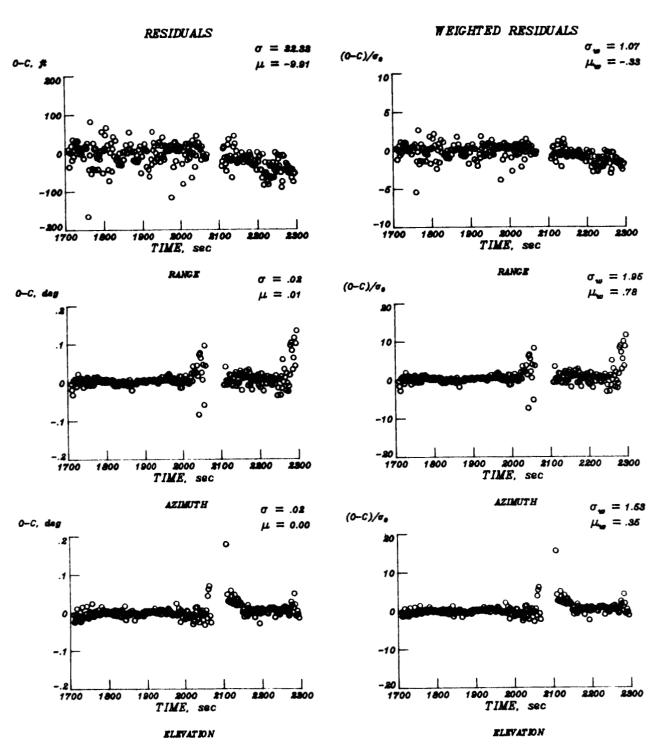


Fig. B-7. Smoothed residuals versus time for FRCC

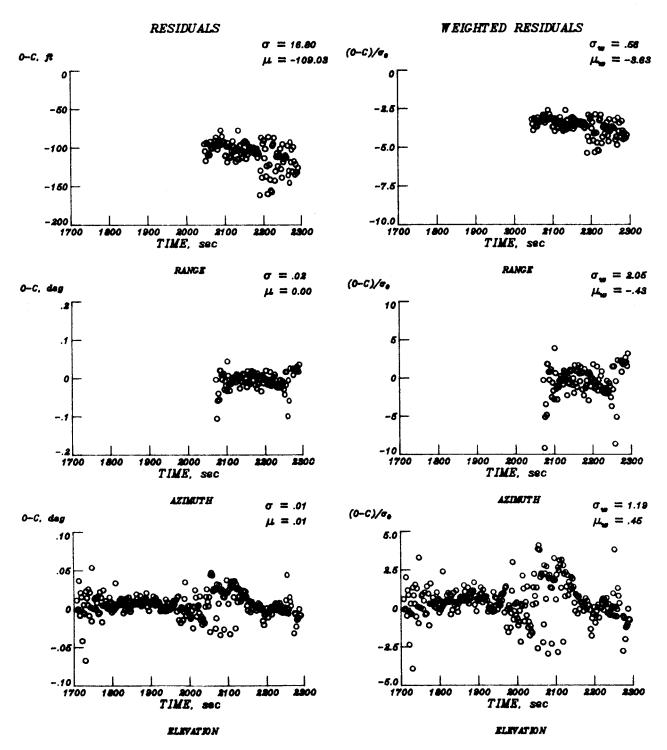


Fig. B-8. Smoothed residuals versus time for EAFC

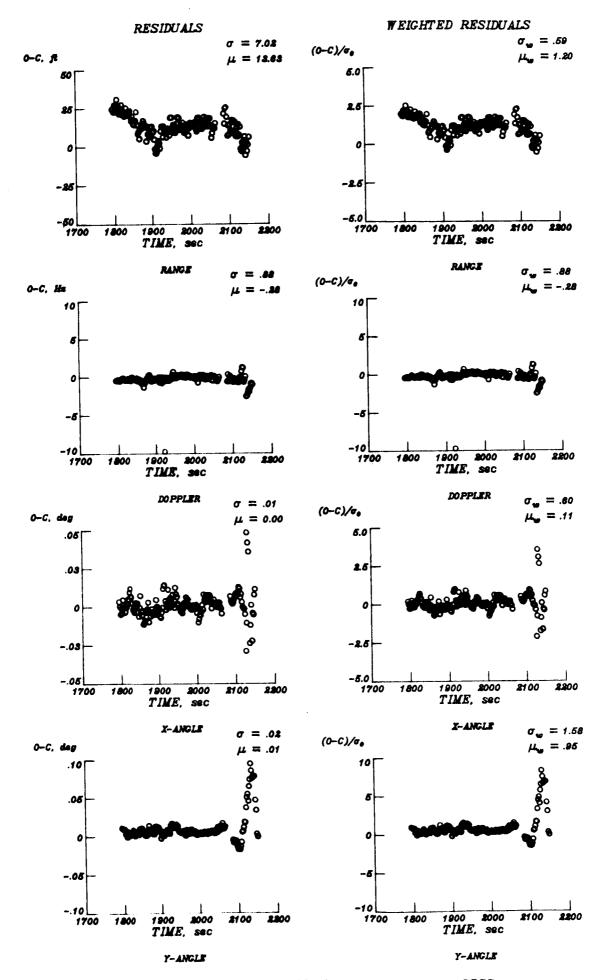


Fig. B-9. Smoothed residuals versus time for GDSS

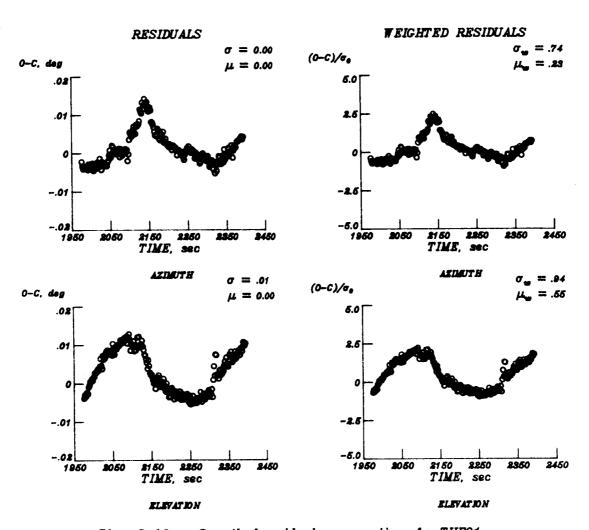


Fig. B-10. Smoothed residuals versus time for THE01

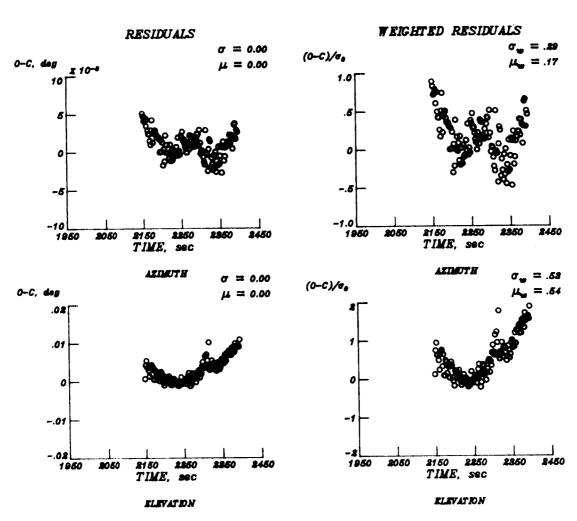


Fig. B-11. Smoothed residuals versus time for THE05

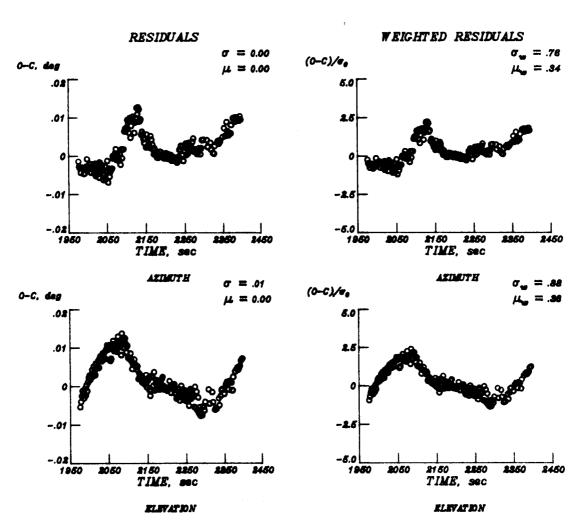


Fig. B-12. Smoothed residuals versus time for THE07

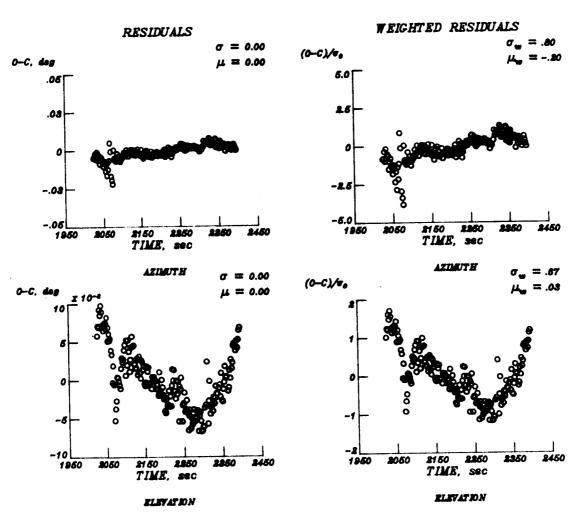


Fig. B-13. Smoothed residuals versus time for THE09

CRIGINAL PACE IS OF POOR QUALITY

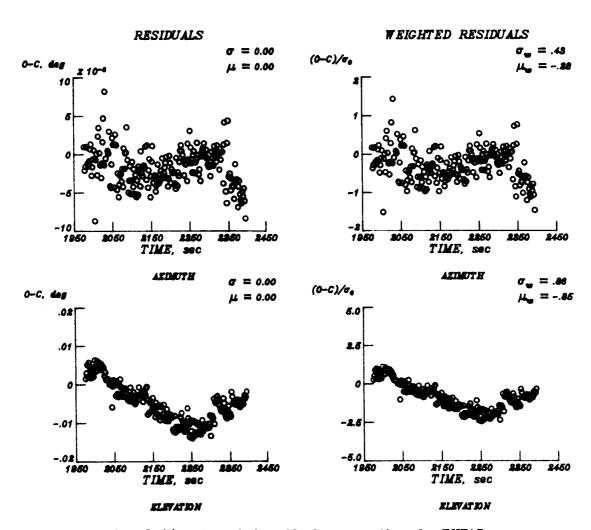


Fig. B-14. Smoothed residuals versus time for THE15

APPENDIX C

Listing of ST14BET air relative parameters @ 2.0 sec

(t, h, V_A , γ_A , ψ_A , σ_A , β_A , α_A , M_A , q_A)

********************************* LARC "EXTENDED" BET HEADER RECORD

									And the same of th
7	-	13	7	5	S M A	1	AHA	U	
(SEC)	(FT)	(FPS)	(386)	(DEG)	(DEG)	(DEG)	(030)	I	(PSF)
	64971	4077	άÇ	9.76	66	.20	1.37	3.17	Ö
0	467892.5	2*079*0	-1.290	59.772	-1.942	1.197	31.523	13,185	000
•	66812	4080	1.29	4.77	1.76	.27	1.71	3.19	Ö
•	65731	4041.	1.29	9.78	1.59	.35	1.90	3.19	Ö
•	04644	4083	29	9.78	.42	.43	2.11	3.20	0
c	635bb.	4084	1.29	9.79	1.25	.50	2.32	3.21	0
	62483	4.085	1.29	9.79	1.10	.58	2.54	3.22	0
,	61398	4087	1.29	9.79	.95	•65	2.76	3.22	0
	60313	4688	1.29	9.80	, C)	.74	3.00	3.23	0
6	59227	4080	1.29	9.81	5	.82	3.24	3.24	0
	58141	4091.	1.30	9.81	~	.89	3.49	3.25	Ō
, ,	57053	4092	1.30	9.82	Ø	96.	3.75	3.26	0
, ,	55965	4004	30	9.82	4	•06	4.02	3.89	Ö
•	54876.	4095	1.30	9.83	3	.13	4.29	3.90	0
000	53786.	4096.	1.30	9.83	0	.22	4.58	3.91	0
0	52696.	4098	1.30	9.84	n	•30	4.87	3.92	0
,	51604	4000	30	9.85	5	•39	5.16	3.92	0
4	50512	4100.	1,30	9.85	~	.46	5.47	3.93	0
36.	49420	4102.	1.30	9.86	7	.55	5.79	3.94	0
38	48326	4103.	1,31	9.86	œ	•64	6.11	3.95	0
707	47232	4104	1.31	9.87	0	.73	94.9	3.96	0
42	46137	4106.	1.31	9.88	ာ	.82	6.79	3.96	0
7 7	45041.	4107.	1,31	9.89	Э-	.91	7.14	3.97	0
9	43945	4109.	1.31	9.89	8	.92	7.51	3.98	ပ
9	42848	4110.	1.31	9.90	~	.92	7.89	3.99	0
50.	41750.	4111.	1.31	16.6	4	.92	92.8	4.00	Ö
2	40652	4113.	1.31	16.6	O	.91	8.55	4.00	0
54	39553	4114.	1,31	9.92	()	.91	8.78	4.01	0
•	36453	4115.	1,31	9.93	Ŋ	.91	8.96	4.02	0
00	37353.	4117.	16	76.6	3	06.	9.14	4.03	0

East approximate transfer for the control of the co

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TIME	ALTOE	VELA	GAMA	HDGA	SIGHAA	BETAA	AL PHAA	MACHA	40
SE	FT)	Sa	U.	يد	DEG	<u>بر</u> د	ָ היי	1	0
•	30252.	4118.	32	9.95	∞	.90		14.043	000
2	35150.	4120.	.32	96.6	4	• 90	44.0	4.05	00
4	34048	4121.	.32	95.6	S	999	0.60	4.06	00
	32945	4122.	.32	9.97	5	.88	9.76	4.06	0
• a	31841.	4124.	.32	96.6	3	.87	76.6	4.07	0
	30737	4125.	.32	66.6	8	.87	0.07	4.08	၁
	29632	4127.	.32	00.0	8	•86	0.20	4.09	0
4	28527	4128.	.32	0.01	3	.86	0.34	4.10	00
	27420	4129.	1.32	0.02	9	.85	0.50	4.11	00
	26314.	4131.	1.32	0.03	O	.82	99.0	4.12	0
•	25206	4132.	1.32	0.04	3	.81	0.83	4.13	8
2	24098	4133.	.33	0.05	9	.80	1.01	4.14	0
•	22496.	4135.	1.33	0.06	0	980	1.03	4.15	C
Ġ	21881.	4136.	1.33	0.07	~	•79	1.06	4.16	0
988	620771.8	24138.1	-1.334	60.082	155	2.777	0	11	S
0	19651.	4139.	.33	0.09	4	•76	1.13	4.18	0
	18550	4140.	1.33	0.10	3	.73	1.18	4:19	0
4	17439.	4142.	1.33	0.11	~	.72	1.23	4.20	0
	16327	4143.	1.33	0.12	0	.71	1.30	4.20	0
œ	15215	4145.	1.33	0.13	0	• 68	1.38	4.21	0
000	14132.	4146.	.33	0.14	0	• 66	1.46	4.22	0
000	12988.	4147.	.33	0.15	0	•64	1.56	4.23	Ò
90	11874	4149.	33	0.16	ာ	•62	• 66	4.25	Ö
•	10750.	4150.	.33	0.18	~	.59	1.77	4.26	0
08	09644.	4152.	.34	0.19	~	.57	1.89	.27	0
10.	08529.	4153.	.34	0.20	.23	.54	.01	00	Ō
2	67413	4154.	•34	0.21	4	.51	2.15	• 50	0
7 7	06296	4156.	34	0.22	.47	.48	2.29	.30	Ö
• • • • • •	05170	4157	34	0.24	5.58	.45	2.45	-	Ö
•		•		•		1 4 4 4			

### ##################################	DATA.	PAGE +++++	* * * * * * * * * * * * * * * * * * * *
ALTDE VELA GAMA HDGA SIGMAA BETAA HDGA (FT) (FFS) (DEG) (DEG			
(FF) (FPS) (DEG) (FTAA AI PHA	ن	
02943.5 24160.5	(DEG)	£	(PSF)
9546.9 24161.9 -1.345 60.278 -1.971 2.34 60.756.3 24164.7 -1.345 60.304 -2.239 2.22	.385 42.79	4.33	0
667058 24164.7 -1.345 60.291 -2.102 2.28 95465.2 24164.7 -1.345 60.304 -2.239 2.22 39545.7 24164.7 -1.345 60.318 -2.539 2.22 39513.3 -1.349 60.331 -2.530 2.13 9513.3 524170.3 -1.349 60.332 -2.566 2.03 9319.5 24170.3 -1.349 60.372 -2.967 2.03 93913.5 24171.7 -1.350 60.400 -3.269 2.03 939813.7 24174.5 -1.350 60.400 -3.269 1.98 87242.4 24176.0 -1.351 60.414 -3.747 1.98 87242.4 24177.3 -1.352 60.443 -3.747 1.98 87242.4 24180.2 -1.353 60.468 -3.747 1.85 86117.7 24181.6 -1.353 60.468 -4.425 1.55 86117.7 24181.6 -1.355 60.598 -4.425 1.55 8737 1.35 80.438.9 24187.2 -1.355 60.599 -4.425 1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.357 60.580 -5.330 1.057 81615.4 24192.3 -1.358 60.662 -6.093 8.00 80.662 -6.297 8.260 -6.207 8.2	34	14.345	0000
99586.3 24164.7 -1.346 60.304 -2.239 2.20 98466.2 24166.1 -1.347 60.318 -2.382 2.21 97345.7 24167.5 -1.347 60.318 -2.382 2.21 97345.7 24167.5 -1.348 60.344 -2.666 2.13 95103.5 24170.3 -1.349 60.372 -2.967 2.09 92859.5 24174.5 -1.350 60.404 -3.269 2.09 91736.9 24174.5 -1.350 60.404 -3.269 1.938 91736.9 241777.3 -1.350 60.404 -3.269 1.938 91736.9 24177.3 -1.350 60.404 -3.269 1.938 91736.9 24177.3 -1.352 60.463 -3.747 1.76 84922.7 24181.6 -1.352 60.463 -3.747 1.76 84922.7 24187.2 -1.355 60.518 -4.075 1.51 884992.7 24187.2 -1.356 60.503 -4.425 1.51 884936.9 24196.9 -1.356 60.503 -4.425 1.51 91834.8 -1.357 60.596 -5.330 1.077 9172.2 24196.9 -1.358 60.663 -5.330 1.077 9172.6 24196.9 -1.358 60.663 -5.330 1.077 9172.6 24198.6 -1.359 60.662 -6.297 -6.297 77464.5 24198.6 -1.359 60.662 -6.297 -6.297 77464.5 24198.6 -1.359 60.662 -6.297 -6.297 77464.5 24198.6 -1.359 60.662 -6.297 -6.297 -6.297 77464.5 24198.6 -1.359 60.662 -6.297 -6.297 -6.297 77464.5 24198.6 -1.359 60.662 -6.297 -6.297 -6.498 -1.359 60.662 -6.297	.314 43.15	4.35	0
96406.2 24166.1 -1.347 60.318 -2.382 2.21 97345.7 24167.5 -1.347 60.331 -2.530 2.17 96224.6 24168.9 -1.348 60.358 -2.666 2.13 93981.7 24171.7 -1.349 60.372 -2.967 2.03 92859.5 24173.1 -1.350 60.400 -3.269 1.93 92859.5 24174.5 -1.350 60.400 -3.269 1.93 90136.9 24176.0 -1.350 60.403 -3.424 1.88 9440.6 24178.8 -1.35 60.472 -4.075 1.70 86117.7 24181.6 -1.35 60.472 -4.075 1.65 86271.5 24186.4 -1.35 60.503 -4.677 1.70 86271.5 24186.7 -1.35 60.503 -4.075 1.65 86772.9 24196.7 -1.35 60.596 -5.30 1.03 77302.8 24196.8 -1.35 60.696 -5.30 1.03 77107.3 24196.8 -1.35 60.696 -5.30 1.07 77507.3 24196.8 -1.35 60.696 -5.30 1.07 77507.3 24196.8 -1.35 60.696 -5.30 1.07 77507.3 24196.8 -1.35 60.696 -5.297 -6.596	.268 43.35	4.36	0
97345.7 24167.5 -1.348 60.331 -2.550 2.17 96224.6 24168.9 -1.348 60.372 -2.666 2.13 93981.7 24171.7 -1.349 60.372 -2.967 2.03 93981.7 24171.7 -1.350 60.372 -2.967 2.03 92859.5 24174.5 -1.350 60.400 -3.269 1.98 91736.9 24177.3 -1.350 60.414 -3.424 1.82 87242.4 24177.3 -1.352 60.443 -3.747 1.82 88117.7 24181.6 -1.352 60.463 -3.912 1.70 86117.7 24181.6 -1.353 60.472 -4.253 1.65 86117.7 24181.6 -1.355 60.598 -2.077 1.356.9 24187.2 -1.356 60.598 -2.076 1.357 60.580 -2.073 1.05 88234.8 24192.9 -1.358 60.613 -2.766 1.357 60.659 -2.093 1.1537 77107.3 24192.9 -1.358 60.613 -5.330 1.15 72593.7 24198.6 -1.359 60.662 -6.297 -6.596 72593.7 24198.6 -1.359 60.662 -6.297 -6.596	.218 43.55	4.37	0
95103.6 24170.3 -1.348 60.358 -2.666 2.13 95103.5 24170.3 -1.349 60.372 -2.809 93981.7 24171.7 -1.349 60.372 -2.967 2.09 92859.5 24173.1 -1.350 60.400 -3.269 1.98 91736.9 24177.3 -1.350 60.400 -3.269 1.98 91736.9 24177.3 -1.351 60.414 -3.424 1.88 8130c.6 24178.8 -1.352 60.443 -3.747 1.88 84932.7 24183.0 -1.353 60.472 -4.075 1.658 849492.7 24183.0 -1.354 60.487 -4.253 1.658 82341.5 24185.8 -1.355 60.593 -4.075 1.38 81615.4 24197.2 -1.355 60.596 -5.330 1.95 77107.3 24192.9 -1.357 60.565 -5.143 1.23 78234.8 24194.3 -1.357 60.565 -5.003 77107.3 24194.3 -1.357 60.596 -5.300 1.07 75979.4 24194.3 -1.359 60.665 -6.093 72593.7 24198.6 -1.359 60.662 -6.093 72593.7 24198.6 -1.359 60.662 -6.093 72593.7 24198.6 -1.350 60.679 -6.506	.171 43.77	4.38	0
95103.5 24170.3 -1.349 60.358 -2.869 2.09 92859.5 24171.7 -1.350 60.372 -2.967 2.03 92859.5 24174.5 -1.350 60.400 -3.269 1.98 921736.9 24174.5 -1.350 60.404 -3.424 1.88 94450.4 24177.3 -1.352 60.443 -3.747 1.82 87242.4 24177.3 -1.352 60.443 -3.747 1.82 887242.4 24177.3 -1.353 60.443 -3.747 1.82 887242.5 24181.6 -1.353 60.472 -4.253 1.58 887242.5 24183.0 -1.355 60.503 -4.425 1.58 88738.9 24185.8 -1.355 60.518 -4.650 1.44 88234.8 24187.2 -1.356 60.580 -5.330 1.15 78234.8 24192.9 -1.357 60.580 -5.330 1.12 77107.3 24194.3 -1.359 60.665 -5.143 1.23 7851.2 24198.6 -1.359 60.662 -6.093 -6.506	.137 43.94	4.40	0
93981.7 24171.7 -1.350 60.372 -2.967 2.03 92859.5 24174.5 -1.350 60.400 -3.269 1.98 91736.9 24176.0 -1.351 60.414 -3.424 1.88 94430.4 24177.3 -1.352 60.428 -3.587 1.82 84430.4 24177.3 -1.352 60.443 -3.747 1.82 87242.4 24187.2 -1.353 60.463 -3.912 1.70 84932.7 24181.6 -1.353 60.487 -4.253 1.55 84932.7 24187.2 -1.355 60.503 -4.425 1.55 8234.8 24187.2 -1.356 60.503 -4.425 1.51 78234.8 24192.9 -1.356 60.565 -5.143 1.23 78234.8 24192.9 -1.357 60.565 -5.143 1.23 78232.6 24197.2 -1.359 60.663 -6.093 .91 73722.6 24198.6 -1.359 60.662 -6.093 .91 7464.5 24108.6 -1.359 60.662 -6.093 .91	.093 44.11	4.41	0
92859.5 24174.5	.036 44.29	4.42	0
91736.9 24174.5 -1.350 60.400 -3.269 1.93 94736.9 24177.3 -1.351 60.414 -3.424 1.88 64434 24177.3 -1.352 60.443 -3.747 1.70 87242.4 24177.3 -1.352 60.443 -3.747 1.70 87242.4 24130.2 -1.353 60.472 -4.075 1.05 86117.7 24181.6 -1.353 60.487 -4.253 1.58 84932.7 24184.4 -1.355 60.503 -4.425 1.58 82741.5 24187.2 -1.355 60.518 -4.600 1.44 81615.4 24187.2 -1.355 60.549 -4.958 1.31 80438.9 24196.7 -1.356 60.549 -4.958 1.31 7322.0 24190.1 -1.357 60.565 -5.143 1.23 74851.2 24197.2 -1.358 60.613 -5.706 -99 77573.4 24198.6 -1.359 60.665 -6.093 -6.506	94.46	4.43	0
90613.9 24176.0 -1.351 60.414 -3.424 1.88 63450.4 24177.3 -1.352 60.428 -3.587 1.82 1.82 1.82 1.82 1.82 1.82 1.82 1.82	.937 44.60	4.44	0
69440.4 24177.3 -1.352 60.463 -3.587 1.82 89360.6 24178.8 -1.352 60.463 -3.747 1.76 87242.4 24180.2 -1.353 60.472 -4.075 1.70 86117.7 24181.6 -1.353 60.487 -4.075 1.65 86492.7 24183.0 -1.354 60.487 -4.253 1.51 84992.7 24184.4 -1.355 60.503 -4.425 1.51 82741.5 24184.4 -1.355 60.518 -4.425 1.51 82741.5 24187.2 -1.356 60.549 -4.958 1.31 78234.8 24196.7 -1.357 60.549 -4.958 1.23 78234.8 24191.5 -1.359 60.659 -5.143 1.23 74651.2 24194.3 -1.359 60.659 -5.09 -9.10 72593.7 24198.6 -1.359 60.662 -6.093 -8.20 72593.7 24198.6 -1.359 60.662 -6.093 -8.20 72693.7 24198.6 -1.3	.880 44.74	4.45	Ü
89362.6 24178.8 -1.352 60.443 -3.747 1.76 87242.4 24180.2 -1.353 60.458 -3.912 1.70 86117.7 24181.6 -1.353 60.472 -4.075 1.65 84,92.7 24184.4 -1.354 60.487 -4.253 1.58 82741.5 24184.4 -1.355 60.503 -4.425 1.51 82741.5 24184.4 -1.355 60.518 -4.425 1.51 82741.5 24187.2 -1.356 60.549 -4.425 1.51 81615.4 24187.2 -1.356 60.549 -4.425 1.31 804.88.9 24186.7 -1.356 60.549 -4.425 1.31 78234.8 24190.1 -1.357 60.549 -5.958 1.31 7107.3 24191.5 -1.358 60.659 -5.520 1.07 74851.2 24194.3 -1.359 60.662 -5.903 -91 72593.7 24198.6 -1.359 60.662 -5.903 -91 72593.7 24198.6 -1.359 </td <td>.826 44.91</td> <td>4.47</td> <td>0</td>	.826 44.91	4.47	0
87242.4 24180.2 -1.353 60.458 -3.912 1.70 86117.7 24181.6 -1.353 60.472 -4.075 1.65 8492.7 24183.0 -1.354 60.487 -4.253 1.58 82741.5 24184.4 -1.355 60.503 -4.425 1.51 82741.5 24187.2 -1.356 60.518 -4.425 1.51 81615.4 24187.2 -1.356 60.549 -4.425 1.51 79362.0 24186.7 -1.356 60.549 -4.425 1.51 79362.0 24190.1 -1.357 60.565 -5.143 1.23 78234.8 24191.5 -1.357 60.580 -5.330 1.15 74851.2 24194.3 -1.358 60.659 -5.330 1.15 74851.2 24194.3 -1.359 60.629 -5.903 91 72593.7 24198.6 -1.359 60.669 -6.903 91 72593.7 24198.6 -1.350 60.669 -6.909 -6.506 72693.7 24198.6 -1.350 <td>.768 45.07</td> <td>4.48</td> <td>٠</td>	.768 45.07	4.48	٠
86117.7 24191.6 -1.353 60.472 -4.253 1.58 84972.7 24184.4 -1.354 60.503 -4.425 1.58 63857.3 24184.4 -1.355 60.518 -4.425 1.51 82741.5 24185.8 -1.355 60.518 -4.600 1.44 81615.4 24187.2 -1.356 60.549 -4.600 1.44 80438.9 24186.7 -1.357 60.549 -4.958 1.31 78234.8 24190.1 -1.357 60.580 -5.143 1.23 73234.8 24192.9 -1.358 60.659 -5.330 1.15 74851.2 24194.3 -1.358 60.659 -5.903 -91 74851.2 24195.8 -1.359 60.669 -6.093 -82 72593.7 24198.6 -1.359 60.665 -6.093 -82 7464.5 24200.0 -1.350 60.662 -6.506 -6.506	.709 45.25	4.49	0
84492.7 24184.4 -1.354 60.487 -4.253 1.58 63807.3 24184.4 -1.355 60.503 -4.425 1.51 823627.3 24185.8 -1.355 60.518 -4.600 1.44 82741.5 24185.8 -1.355 60.518 -4.600 1.44 82741.5 24196.7 -1.356 60.549 -4.777 1.38 80438.9 24196.1 -1.357 60.549 -4.958 1.31 73224.8 24192.9 -1.357 60.580 -5.330 1.15 7107.3 24192.9 -1.358 60.613 -5.766 -9.97 7222.6 24197.2 -1.359 60.662 -5.903 -5.903 72522.6 24197.2 -1.359 60.665 -6.093 -6.297 72593.7 2464.5 24198.6 -1.360 60.665 -6.297 73	.651 45.40	4.50	0
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82741.5 24185.8 -1.355 60.518 -4.600 1.44 81615.4 24187.2 -1.356 60.533 -4.777 1.38 80438.9 24186.7 -1.356 60.549 -4.958 1.31 79362.0 24190.1 -1.357 60.565 -5.143 1.23 78234.8 24191.5 -1.357 60.580 -5.330 1.15 77107.3 24192.9 -1.358 60.613 -5.706 .99 75979.4 24194.3 -1.358 60.613 -5.706 .99 74851.2 24195.8 -1.359 60.629 -5.903 .91 73722.6 24197.2 -1.359 60.645 -6.093 .82 72593.7 24198.6 -1.360 60.645 -6.506 .64	.512 45.67	4.53	0
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	MACHA	Ĵ:	4.76	4.72	4.73	4.74	4.76	4.77	4.79	4.80	4.82	4.83	4.85	4.86	4.88	4.90	4.91	4.93	4.94	96.4	4.98	66.4	5.01	5.03	5.05	5.06	5.08	5.10	5.12	5.13	15,158	
:	A H d	(DEG)	8.84	9.25	9.70	9.85	9.19	8.59	8.02	7.53	7.06	6.62	6.24	5.85	5.35	4.59	3.86	3.14	2.41	1.73	1.71	1.70	1.70	1.76	1.86	1.80	1.71	1.49	1.27	1.08	40.893	
	T A	(056)	844.	.342						9		4	0	.02	Œ	1.16	•23	~	0	8	~	N	4	Ō	N	~	9	-	Œ	~	.155	•
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	90	(DEG)	0.71	0.73	97.0	6.79	0.78	0.80	0.81	0.83	0.85	0.87	0.89	0.91	0.92	90.0	96.0	0.98	1.00	1.02	1.04	1.06	1.08	1.10	1.12	1.14	1.16	1.18	1.20	1.23	61.251	1
	AMA	(056)	1.36	1.36	1.36	1.36	1.36	1.36	1.36	-	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.36	1.37	1.37	-1.370	
	VEL	(FPS)	4202	4204	4205	4207	4208	4209	4211.	4212	4214.	4215.	4217	4218.	4219.	4221.	4222.	4224.	4225.	4227	4228	4230	4231.	4233.	4234.	4235.	4237	4238.	4240.	4241.	24242.9	
	_	(FT)	69205	6 K C 74	46646	65813	64683	63552	62421.	61230	6015k	59027	57895	56762	55630.	54498	53365	52232	51099.	49666	48632	47698	46564	45430.	44295	43101.	42626	40.692	39757.	38622	537487.3	
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(SEC)	(FT)	(FPS)	(1)	(DEG)	(DEG)	(DEG)	(050)		(PSF)
! !					(i d		0
40.	35216.	4245	1.37	1.29	300	→	* C • C	7 - 7	
6.0	34(.81	4247.	1.37	1.31	03	27	0.42	5.21	0
. 77	22065	4248	1.37	1.33	. •	3	0.30	5.23	00
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	していると	4253	1.37	1.40	~	56	6.00	5.29	0
) (7,447	4254	1.37	1.42	~	40	06.6	5.31	0
, v , v	27256	4755	1.37	1.44	m	34	9.85	5.33	0
, v	26740	4257	1.37	1.47	· O	.16	9.82	5.35	00
	5,4694.5	24258.7	-1.372	61.495	354	.011	39.803	15.372	100.
	23858	4260.	1.37	1.51	0	17	9.78	5.39	0
6 2 9	22722	4261.	1.37	1.54	0	28	9.77	5.41	2
4	21585	4263.	1.37	1.56	~	03	9.18	5.43	0
. 4	20440	4264	1.37	1.58	4	18	9.78	5.45	0
• ·	19313	4265.	1.37	1.61	Œ	39	9.80	5.47	9
70.	18:76.	4267.	1.37	1.63	Q.	60	9.84	5.50	00
7.5	17040	4268	1.37	1.65	O	21	96.6	5.52	00
76.	15904	+270.	1.37	1.63	2	16	9.08	5.54	00
76.	14767	4271.	1.37	1.70	•	08	0.09	5.56	0
8	13631	4273.	1.37	1.73	O	0	0.20	5.59	O
• 0	12404	4274.	1.37	1.75	. ^	~	0.32	5.61	0
• 0 • 0	11256	4275	1.37	1.78	ပ	S	0.42	5.63	0
) Q	10221	4277.	1.37	1.80	4	E	0.58	5.66	\circ
• 4	000000	4278	1.37	1.93	60.	~	0.73	5.68	0
• • •	07070	1280	1.37	1.85	.23	0	0.89	5.70	\circ
• 0 0	0.55	4281	1.37	1.88	1.41	O	1.05	5.73	0
	0244	4283	1.37	1.90	1.31	. 7	1.22	5.75	0
• · · ·	57440	4284	1.37	66.1	15	~	1.21	5.78	0
•	90770	4704	1.37	1.95	N	0	1.19	5.80	0
• C : C D : 4	00000	4287	1.37	1.98	.91	4	1.17	5.83	0
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. ; ((-)	8.22	8.28	8.34	8.40	8.46	8.53	8.59	8.66	8.72	8.79	8.86	8.93	00.6	9.08	9.15	9.23	19.310	9.38	4.47	9.55	6.63	9.72	08.6	68.6	86.6	0.07	0.16	0.25	0.35	77.0
	(DEG)	96.0	0.91	0.91	0.87	0.83	0.80	0.79	0.78	0.79	0.84	0.89	0.95	1.00	0.95	0.91	0.87	40.855	0.83	0.83	0.83	0.83	0.85	0.87	06.0	0.92	76.0	0.89	0.83	0.10	0.78
*	(DEC)	.38	44.	~	.21	Q	0	4	O	-	'n	•	0	~	~	•04	m	.124	0	~	4	B	-	0	5	0	~	9	5	~	Ä
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((DEG)	3 . 85	3.39	3.43	3.96	4.00	4.03	4.07	4.11	4.14	4.18	4.22	4.25	4.29	4.33	4.37	4.40	24.447	4.48	4.52	4.56	4.60	4.63	4.67	4.71	4.75	4.79	4.83	4.87	4.91	4.95
3	() E G)	1.35	1.35	1.35	1,35	1.35	1.35	1.35	1.35	1.35	1.35	1.35	1.35	1,35	1.35	1.35	1.34	-1.349	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34	1.34	.34	34	34
1	VELA (FPS)	4374.	4375	4377	4378	4379.	4381	4382	4394	4385.	4386	4388°	4389.	4391.	4392.	4393.	4395.	24396.7	4398.	4399	4400	4402.	4403.	4405.	4406.	4407	•6075	4410.	4412.	4413.	4414.
(ALTDE (+T)	23336	32218	36078	26976	28861.	27743.	26625	2550k	24391	23275	22159	21044	19929	18615.	17701.	.658R.	415475.8	14363.	13252	12141.	11030.	09921	08611	C7702.	06594	05487	04330	03274	02168	01063
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·T- 6.0444	65.74	77	13	0.24	2.36	02
4442.3 -1.	65.78	39	10	0.22	5.46	0.0
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4450.4 -1.	66.04	.31	.19	0.23	3.09	03
4451.7 -1.	60.99	1.49	25	0.25	3.19	03
4453.1 -1.	66.13	• 66	31	0.28	3.30	03
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4455.7	66.22	03	47	6.34	3.51	4

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A H d	(DFG)	9.64	9.67	9.70	9.72	9.73	9.74	9.74	9.75	9.74	9.73	69.6	9.64	9.57	9.57	9.55	9.52	64.6	9.50	69.6	6.46	68.6	66.6	0.00	0.21	0.34	0.48	0.65	.85	41.068	-26
Y	(050)	0	N	8	3	.39	N	-	~	•	~	-	4	60	•	18	23	5	56	~	œ	0	\sim	~	-4	0	8	9	4	•200	m
GMA	(DEC)	0	.91	1.07	1.25	25	1.23	1.17	96.	7	~	0	~	•	~	œ	0	8	15	~	28	37	S	2	S.	9	3	0	•	.917	3
90	(0EG)	7.68	7.73	7.78	7.83	7.88	7.93	7.98	8.03	d. JE	8.13	8.18	8.23	8.26	8.34	8.39	44.0	9.49	8.54	8.59	8.65	8.70	8.75	8.81	8.86	8.91	96.9	9.02	9.07	69.129	9.18
X.	(DEC)	1.27	1.27	1.27	1.27	1.27	1.26	1.26	1.26	1.26	1.26	1.26	1.25	1.25	1.25	1.25	1.25	1.24	1.24	1.24	1.24	1.24	1.23	1.23	1.23	1.23	1.22	1.22	1.2	-1.221	1.2
	(FPS)	7077	400F	4044	4408	6655	450C.	4501.	4502	4503.	4504	4505	4506.	4507	4508	4509	4510.	4511	4512	4513	4513.	4514.	4515.	4516.	4516.	4517.	4518.	4518.	4519.	24520.1	4520
* -	(FT)	(人) () () ()	340.46	10067	31066	30538	2085	/B. 5.56 -	27762	20715	25677	24637	23598	22561	2,526.	20407	16450	15478	17399	16372	15346	14322	13300.	12231	11263	10247	09233	04221	07211.	306203.9	S A C R C R C
X	(SEC)	•	0 0	• J 4		٠ س د د		, ~	7 -	4	8	200	22.	24.	. 4	0 00	30	י ער	1 4	, v	0 C			7 7	4.4	α	50.	300	56	656.0	i c

STI4BET USING ST144ET(11/34), INFRTIAL-BT14NOZ, NB1060 DYN. DATA.

0A (PSF)	000	200	W 4 4	83.4	200	2.468 2.756 2.911 2.012	242 419 603 796	6 4 2 9 6 4 2 9 6 4 8 2 3 5 6 8
MACHA (-)	7.20	7.21	7.22	7.22	2	27.727 27.773 27.816 27.853	96.7	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
ALPHAA (DEG)	6.83 6.83 1.33 1.33	1.24	0.88 0.72 0.52	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	9.02	200 200 200 200 200 200 200 200 200 200	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
BETAA (DEG)	000 0 0 0 0	22.0	22.2	2000	52	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	0 @ m @ @
SIGMAA (DEG)	400	99	. 42. . 44.	1.02	31 10 10 10 10 10 10 10 10 10 10 10 10 10	1	947	8 7 7 6 6
Н96 A (DEG)	2.63	44.		9.73	0.19	70.219 70.247 70.274 70.305	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.03 0.03 7.00 7.00
G AMA (0EG)	1.21	202-1	1.20 1.19 1.19	1.18	1.15 1.15 1.15 1.15	-1.144 -1.138 -1.133 -1.127	1011 1010 1000	11.08
VFLA (FPS)	521.	522 522	522 522 523 523	522	,522. ,717. ,715.	24737.2 24695.5 24695.5 24689.0 24682.1	4674 4666 4058 4649	4639 4629 4610 4610
ALTDE (FT)	24195. 33195.	12197. 11232. 10210.	99220. 98233. 97240.	95291. 94317. 93347.	92380. 91417. 90458. 89504.	288553.7 287637.9 286660.8 285730.7 284739.8	83874 62954 82040 81132	60231. 79336. 78447. 77566. 76691.
TIME (SEC)	200	φ. φ.	22.5	30.00	4 6 8 0	692.0 694.0 696.0 0.0 0.0 0.0	0 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	100

+ TOPACE TOPACE	***************************************
+ CT14RET DSING ST14MET(11/84), [NERTIAL-BT14N02,NB1060 DYN. DATA.	· 计算量分类的 计多数分类 计多数 计多数分类 计多数分

V O	(PSF)	80	.12	.37	• 63	5.901	.17	4.5	• 74	• 04	.34	65	.97	.29	• 62	96	52.	• 64	9.98	0.33	0.68	1.03	1,38	1.73	2.09	5.44	2.78	3.12	3.46	. 79	4.11
		9.00	1.99	7.98	1.97	27.960	7.94	7.92	7.89	7.87	7.84	7.81	7.78	7.75	7.72	7.69	7.65	7.62	7.58	7.55	7.51	7.47	7.44	7.40	7.36	7.33	7.29	7.25	7.21	7.17	7.14
	0	9.69	0.17	0.71	1.01	41.108	96.0	0.56	0.01	9.62	9.45	9.47	9.68	0.03	0.45	0.83	1.05	1.05	0.84	44.0	9.92	9.52	9,31	9.32	9.56	9.08	0.55	0.99	1.22	1.17	0.84
•	(DEG)	19	8	38	~	420	3	0	27	~	27	9	•	•	•	ω	9	4	~	O	24	-	9	3	18	~	21	ŝ	11	9	25
GMA	(DEC)	9.	•	.21	.02		~	Φ	~	S	_	0	7	2	82	4	• 19	27	10	.79	55	41	32	18	Φ	0	~	O.	ω	Q	S
90	(DEG)	0.17	0.82	0.87	0.92	70.982	1.03	1.09	1.15	1.21	1.27	1,33	1.39	1.45	1.51	1.58	1.04	1.71	1.77	1.84	1.50	1.97	2.04	2.10	2.17	2.24	2.31	2.37	2.44	2.51	.57
I	(056)	1,04	1.04	1.03	1.01	1.00	65.	96	20.	95	40.	.93	16.	06.	α α	.87	φ π)	.84	.82	80	.78	.77	.75	.73	.71	69.	67	65	63	9	585
VEL	(FPS)	45000	4579	4.56.20	4036	4544	4532	4518	4506	7077	4482	4470.	4458	4446.	4435	4424	4412.	4401.	4390	4378	4368	4357	4347	4336.	4325.	4314.	4303	4231	4270	4267	24256.2
-	(FT)	75676	74965	741.6.	73573	77447	7.673	70830	70011	60222	68446	67681	2000 2000 2000 2000	66137	65400	64745	64045	63359	67638	62032	10000	60764	60153	5655R	54979	58415	57471	57263	7.50.00	56245	255875.6
1	(SEC)	Š	, , ,	• 7 C	V V	• 0 0 0 0	9 0		34.	. 4		0	6.0	777	4 4 4	8	2 6	52	1 4	,	י סמ		,	• • • • • •		• a	• • •	2 6	74.	7 4 6	778.0

ST148ET USING ST144ET(11/94), INERTIAL-BT14NC2, NB1060 DYN. DATA.

OA (PSF)	. 43	4.74	5.03	5.32	5.60	5.86	6.12	6.36	6.60	6.82	7.04	7.25	7.45	7.65	7.84	8.02	18.203	8.37	8.54	8.71	8.87	9.02	9.16	9.31	44.0	9.57	9.68	9.79	06.6	00.0
MACHA (-)	7.1	7.06	7.03	7.00	96.9	6.93	9.90	6.87	6.84	6.81	6.78	6.75	6.72	6.70	6.67	6.64	6.61	6.59	6.56	6.54	6.51	6.48	6.46	6.43	6.41	6.39	6.36	6.34	6.31	•2•
ALPHAA (DEG)	0.33	76.6	9.83	96.6	0.22	0.46	0.57	0.42	90.0	9.73	9.46	9.30	9.29	64.6	9.77	0.04	40.203	0.23	0.08	4.97	0.03	0.10	9.84	9.22	9.63	0.19	0.72	1.06	1.07	0.88
BETAA (DEG)	20	14	.31	0	05	07	02	03	60	28	.79	22	03	20	.22	22	7	.33	4	.78	32	22	-	15	15	54	9	19	55	.11
SIGMAA (DEG)	1.42	5.05	10.89	16.83	22.52	28,37	34.31	40.25	46.26	52.22	56.11	58.27	60.64	63.25	05.14	66.52	7.5	44.29	67.71	68.16	66.19	65.13	46.49	04.41	63.76	63.46	66.55	71.69	74.11	75.44
HDGA (DEG)	2.64	2.71	2.77	2.84	2.90	2.95	3.00	3.06	3.10	3,15	3.19	3.23	3.28	3.32	3.36	3.40	3.43	3.47	3.51	3.55	3.58	3.62	3.66	3.70	3.73	3.77	3.81	3.84	3.87	73,911
GAMA (DEG)	rc.		.51	64	47	75	42	9	39	37	36	34	4	32	331	30	(6)	2.9	2 8	27	26	25	2.5	.24	23	. 22	2	0	0	195
VELA (FPS)	4244.	4233.	4222	4211	4200	133	4177	4165	4153.	4141	4130	4118	4107	4005	4004	4071	4059	4046.	4033	4021	4008	3005	3982	3969	1057	3063	3020	3016.	3001	23887.7
ALTDE (FT)	55424	54993	54537	54190	53817	53454	53120	52811	52509	52221	51946	51631	51636.	51181	50044	56716	50494	56.240	50672	40872	40677	40400	4931	4016.)	4 Z Z Z Z Z	45 x 2 3 4	4847E	48527	01701	246272.1
TIME (SEC)	a O	, a	9 00		• • • • • • • • • • • • • • • • • • •			, d	90	• a		, A	1 4	• 4 • 4 • 6			2 -	. 7	. 4		0 0	0 0	74.) a		, ,	• 7 c	• • (838.C

-78.021	78.021 66.147 - 81.135 -	WW44444 	00000000000000	••••••	• • • • • • • • • • • • • •
62.245	66.147 – 81.135 –			103 1195 1196 1196 1196 1200 1200 1210 1210 1210 1210 1210 121	38459.6 38617.2 38617.2 38617.2 38617.2 3773.9 3773.9 3773.9 3773.9 37759.4
81-135231	81.135 -		44444444444444444444444444444444444444	193 193 196 198 198 198 198 198 198 198 198 198 198	3845.6 3845.6 3831.4 -195 74.0 3786.4 -20C 74.1 3773.9 -205 74.1 3715.6 -215 74.2 3715.6 -215 74.2 3671.3 -223 74.3 -223 74.3
61.833178			44444444	195 196 196 206 206 203 208 741 215 215 742 215 742 215 742 215 742 215 742 215 742 215 743	3631.4195 74.0 3817.2196 74.0 3786.420C 74.1 3773.9203 74.1 3759.4206 74.2 3759.4206 74.2 3759.4206 74.2 3759.4208 74.2 3759.4208 74.2 3759.4208 74.2 3759.4208 74.2 3759.3223 74.3 3671.3223 74.3
62.234203	E1.833 -			196 205 205 206 206 206 208 74-1 212 74-2 215 74-2 215 74-2 215 74-2 215 74-2 215 74-2	3817.2196 74. 3786.420C 74. 3773.9203 74. 3759.4206 74. 3715.6212 74. 3715.6212 74. 3715.6222 74. 3671.3223 74.
62.451141 40.922 26.151 20. 62.724167 41.001 26.127 20. 62.928188 41.005 26.078 20. 63.040186 40.970 26.078 20. 63.022292 40.890 26.028 21. 62.618294 40.895 26.003 21. 62.618295 40.895 26.003 21. 61.494324 40.977 25.977 21. 61.494323 41.073 25.873 21. 78.084223 41.073 25.873 22. 76.836223 41.073 25.873 22. 76.836204 40.774 25.686 22. 76.837196 40.774 25.686 22. 76.877166 40.777 25.686 22. 76.877168 40.854 25.659 23. 72.255067 40.839 25.605 23. 72.255067 40.839 25.505 23.	42.234 -		30000mm	203 206 203 203 205 206 215 215 215 215 215 216 216 217 218 218 218 218 218 218	3602.9198 74.1 3786.420C 74.1 3773.9203 74.1 3759.4206 74.2 3715.6212 74.2 3715.6215 74.2 366.1221 74.3 3656.3223 74.4
62.724 -167 41.001 26.103 20. 82.928 -186 40.970 26.078 20. 83.020 -227 40.917 26.053 21. 83.022 -292 40.890 26.028 21. 82.616 -294 40.895 26.003 21. 82.108 -295 40.895 25.977 21. 81.494 -324 40.977 25.956 21. 80.738 -223 41.018 25.926 21. 78.874 -223 41.073 25.874 22. 76.806 -223 41.073 25.876 22. 76.836 -215 40.976 25.879 21. 76.836 -25.776 22. 22. 22. 76.836 -25.776 22. 22. 22. 76.837 -219 40.854 25.740 22. 76.837 -219 40.744 25.766 22. 74.877 -25.766 25.740 22. 74.877 -26.766 25.740	82,451 -		444444	205 203 203 206 206 208 212 212 742 215 742 215 743	3786.420C 74.1 3773.9203 74.1 3759.4206 74.2 3744.9206 74.2 3715.6212 74.2 3715.6212 74.2 3656.3221 74.3 3656.3223 74.3
82.928 -188 41.005 26.103 20. 83.040 -186 40.970 26.053 21. 83.022 -227 40.917 26.053 21. 82.618 -294 40.977 25.977 21. 82.108 -324 40.977 25.952 21. 81.494 -324 40.977 25.952 21. 80.738 -323 41.018 25.977 21. 79.800 -223 41.018 25.873 21. 79.804 -223 41.055 25.873 22. 76.874 -215 40.976 25.899 21. 76.836 -219 40.854 25.740 22. 75.597 -196 40.744 25.766 22. 75.597 -196 40.744 25.766 22. 74.257 -106 40.777 25.686 22. 74.257 -106 40.774 25.659 23. 73.650 -204 40.862 25.635 23. 72.555 -009 40.852 25.555 23.	£2.724 -		44444	203 206 206 208 212 212 74-2 215 74-2 215 74-2	3773.9203 74.1 3759.4266 74.2 3744.9206 74.2 3715.6212 74.2 3700.9218 74.3 3671.3223 74.3
83.040186	82.928		4444	206 74.2 208 74.2 212 74.2 215 74.2 218 74.3	3759.4206 74.2 3744.9208 74.2 3715.6212 74.2 3715.6215 74.3 3686.1221 74.3 3671.3223 74.4
83.121 227 40.917 26.028 21. 83.022 294 40.895 26.003 21. 82.66 294 40.895 26.003 21. 82.108 295 40.977 25.977 21. 81.494 324 40.977 25.956 21. 80.738 323 41.018 25.926 21. 79.800 287 41.055 25.873 21. 78.874 223 41.055 25.873 22. 76.806 215 40.976 25.887 22. 76.807 219 40.976 25.786 22. 76.807 296 40.774 25.766 22. 74.877 256 40.777 25.686 22. 74.877 158 40.777 25.659 23. 72.565 099 40.824 25.659 23. 72.565 099 40.839 25.659 23. 72.565 067 40.824 25.555 23. 72.555	83.046	-4	444	212 212 74-2 215 74-2 218 74-3 221 74-3	3744.9208 74.2 3730.3212 74.2 3715.6215 74.3 3685.1221 74.3 3671.3223 74.3
83.022 40.895 26.028 21. 82.618 294 40.895 26.003 21. 82.108 295 40.928 25.977 21. 81.494 324 40.977 25.952 21. 80.738 323 41.018 25.958 21. 79.800 287 41.018 25.873 21. 78.084 223 41.073 25.873 21. 76.836 215 40.976 25.873 22. 76.836 215 40.954 25.766 22. 76.837 219 40.744 25.766 22. 76.877 219 40.744 25.766 22. 74.257 196 40.777 25.686 22. 74.257 173 40.862 25.659 23. 72.565 099 40.862 25.659 23. 72.252 099 40.862 25.659 23. 72.252 099 40.862 25.555 23. 72.252 067	83,121 -		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	212 74.2 215 74.2 218 74.3 221 74.3	3730.3212 74.2 3715.6215 74.2 3700.9218 74.3 3686.1221 74.3 3671.3223 74.3
62.616 294 40.895 26.003 21. 62.108 295 40.977 25.977 21. 61.494 324 40.977 25.952 21. 80.738 323 41.018 25.952 21. 79.800 287 41.055 25.873 21. 78.874 223 41.055 25.873 22. 76.846 215 41.063 25.873 22. 76.846 215 40.976 25.820 22. 76.836 219 40.854 25.766 22. 76.877 246 40.777 25.768 22. 74.257 173 40.777 25.659 23. 72.557 204 40.862 25.659 23. 72.555 099 40.862 25.659 23. 72.252 099 40.862 25.558 23. 72.252 099 40.862 25.557 23. 72.252 099 40.862 25.555 23. 72.252	83.022	4	4.2	215 74.2 218 74.3 221 74.3	3715.6215 74.2 3700.9218 74.3 3686.1221 74.3 3671.3223 74.3
82.108 295 40.928 25.952 21.8 81.494 324 40.977 25.952 21.8 80.738 323 41.018 25.926 21.7 79.800 287 41.018 25.873 21.7 78.874 215 41.055 25.873 22.8 76.836 215 40.976 25.820 22.8 76.836 219 40.954 25.766 22.8 76.836 246 40.744 25.766 22.7 76.836 246 40.777 25.766 22.7 74.257 173 40.777 25.686 22.7 73.656 204 40.862 25.659 23.8 72.555 099 40.862 25.659 23.8 72.252 067 40.862 25.659 23.8 72.252 067 40.862 25.659 23.8 72.252 067 40.862 25.557 23.8 72.552 067 40.862 25.557 23.8 <tbod< td=""><td>82.618</td><td>ις.</td><td>4.3</td><td>.218 74.3 .221 74.3</td><td>3686.1221 74.3 3671.3223 74.3 3656.3225 74.4</td></tbod<>	82.618	ις.	4.3	.218 74.3 .221 74.3	3686.1221 74.3 3671.3223 74.3 3656.3225 74.4
61.494324 40.977 25.952 21. 60.738323 41.018 25.899 21. 78.874223 41.055 25.873 21. 78.084215 41.063 25.873 21. 78.084215 40.976 25.820 22. 77.472250 40.976 25.793 22. 76.836219 40.854 25.766 22. 74.257166 40.774 25.766 22. 74.257166 40.777 25.686 22. 73.660204 40.854 25.659 23. 72.565099 40.862 25.605 23. 72.555067 40.852 25.578 23. 72.252067 40.852 25.578 23.	82.108 -	9	•	.221 74.3	3671.3223 74.3 3656.3225 74.4
80.738 323 41.018 25.926 21. 79.800 287 41.055 25.873 21. 78.874 223 41.055 25.873 21. 78.084 215 41.063 25.846 22. 77.472 250 40.976 25.846 22. 76.207 196 40.444 25.740 22. 75.597 246 40.774 25.740 22. 74.877 166 40.774 25.740 22. 74.877 166 40.777 25.686 22. 73.656 204 40.824 25.659 23. 72.565 133 40.862 25.659 23. 72.555 099 40.862 25.578 23. 72.252 099 40.862 25.578 23. 72.565 067 40.862 25.578 23. 72.061 067 40.862 25.578 23. 72.555 069 40.862 25.555 23.	81.494		4.3		3656.3225 74.4 74.4
79.800287 41.055 25.899 21. 78.874223 41.073 25.873 21. 78.084215 41.063 25.873 21. 77.472250 40.976 25.820 22. 76.836246 40.744 25.740 22. 74.257168 40.777 25.686 22. 74.257173 40.824 25.659 23. 72.565099 40.839 25.605 23. 72.252067 40.846 25.578 23.	86.738	ø	4.3	• • • • • • • • • • • • • • • • • • • •	3656.3225 74.4
78.874223 41.073 25.873 21. 78.084215 41.063 25.846 22. 77.472250 40.976 25.820 22. 76.836219 40.854 25.793 22. 76.207196 40.714 25.793 22. 74.877168 40.777 25.686 22. 74.257173 40.824 25.659 23. 72.565067 40.839 25.605 23. 72.252067 40.826 25.578 23.	79.800	0	4.4	.225 74.4	
78.084215 41.063 25.846 22. 77.472250 40.976 25.820 22. 76.836219 40.854 25.793 22. 76.207196 40.716 25.740 22. 74.257168 40.777 25.686 22. 74.257173 40.777 25.686 22. 73.656204 40.824 25.659 23. 72.555067 40.824 25.655 23. 72.252067 40.824 25.552 23.	78.874 -	o -	4.4	27 74.4	3641.2227 (4.4
77.472250 40.976 25.820 22. 76.836219 40.854 25.793 22. 76.207196 40.744 25.766 22. 76.207246 40.716 25.713 22. 74.877166 40.777 25.686 22. 73.660204 40.824 25.659 23. 72.565099 40.862 25.605 23. 72.252067 40.846 25.578 23. 72.252067 40.846 25.552 23.	78.084		4.4	.228 74.4	3626.1228 74.4
76.836219	77.472 -		4.5	.229 74.5	3610.9229 74.5
76.207196	76.836		4.5	29 74.5	3595.8229 74.5
75.597246 40.716 25.740 22. 74.877168 40.724 25.713 22. 74.257173 40.824 25.686 22. 73.660204 40.824 25.659 23. 73.023133 40.862 25.659 23. 72.565067 40.839 25.605 23. 72.252067 40.626 25.578 23.	76.207	2	4.5	.230 74.5	3590.8230 74.5
74.877168 40.724 25.713 22. 74.257173 40.824 25.686 22. 73.660204 40.824 25.659 23. 73.023133 40.862 25.659 23. 72.565099 40.839 25.605 23. 72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	- 75.597	3	4.6	.230 74.6	3565.8230 74.6
74.257173 40.777 25.686 22. 73.666204 40.824 25.659 23. 73.023133 40.862 25.632 23. 72.565099 40.839 25.605 23. 72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	74.877		4.6	.229 74.6	3550.7229 74.6
73.666204 40.824 25.659 23. 73.023133 40.862 25.632 23. 72.565099 40.839 25.605 23. 72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	74.257		4.6	.229 74.6	3535.5229 74.6
73.023133 40.862 25.632 23. 72.565099 40.839 25.605 23. 72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	73.666 -	ø	4.6	228 74.6	3520.2228 74.6
72.555099 40.839 25.605 23. 72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	73.023 -	9	4.7	74.7	3504.8227 74.7
72.252067 40.746 25.578 23. 72.061099 40.626 25.552 23.	72.565 -	_	4.7	.226 74.7	3489.0226 74.7
72.061099 40.626 25.552 23.	72,252 -		4.7	74.7	3473.6224 74.7
71 772 - 1001 - 101 75 575 73	72.061 -		4	.223 74.B	3458.2 223 74.B
	71.772 -		4 . 8	21 74.8	3442.9221 74.8

ORI	GINAL	PACE	5.3
OF.	POOR	QUALI	7Y

ALTRE	VELA	6 A 4 A	HDGA	SIGMAA	BETAA	ALPHAA	MACHA	V D C E
(FT)	(FPS)	956)	DE G.	() = 6)	940	(920)		
43770.	3427.	.22	4.88	71.42	90.	0.54	7	700
43623.	3412.	.21	16.4	71.06	•00	0.55	2.47	3.98
43477	3396	.21	4.94	70.70	00.	0.58	5.44	4.11
4333	3981	21	4.97	70.61	.05	0.61	5.41	4.24
43303	3365		5.00	70.68	01	0.55	5.39	4.37
**************************************	3369	21	5.03	70.71	10.	9.44	5.36	4.50
24261012	233461	210	75.066	-70.671	•084	40.331	25.340	24.633
4277	4418	20	5.09	70.78	05	0.29	5.31	4.76
42633	2000	200	5.11	76.89	10	0.31	5.28	4.88
40000	2227.	200	5.14	71.02	00	0.34	5.26	5.01
42350	3271	200	5.17	71.12	02	0.38	5.23	5.13
46374	3255	200	5.20	71.21	10.	0.38	5.20	5.26
	3230	200	5.23	71.28	.02	0.30	5.18	5.38
45014	3223	2	5.26	71.34	02	0.18	5.15	5.51
61 2 1 5 c	3207	200	5.29	71.37	00.	0.06	5.12	5.63
4) 0 d 1 e	3191	.20	5.31	71.31	•08	76.6	5.10	5.76
41545	3175	202	5.34	70.95	60.	9.89	5.07	5.88
4 1 4:30	3159		5.37	76.31	90	9.84	5.05	6.01
41 / 73	3142	.20	5.40	69.69	•03	9.76	5.02	6.14
41136	3127	20.	5.43	69.02	œ	99.6	66.4	6.26
41034	3110.	20	5.45	68.20	0	9.57	4.97	6.39
40871	3094	20	5.48	67.40	02	9.55	4004	6.52
40739	3078	.20	5.51	66.86	40	9.55	4.91	6.64
40404	3062	0	5.54	66.38	02	9.54	4.89	6.76
16404	3046	19	5.56	65.86	03	9.54	4.86	6.88
40.505	3029	6.19	5.59	65.31	08	9.49	4.83	7.00
40231	3013	19	5.62	64.92	60	9.48	4.81	7.11
401102	2606	8	5.65	4.67	5	4.47	4.78	7.22
30005	2980.	8	5.68	4.83	4	4.67	4.76	7.33
			1	9	1	67 0	27	777

STI48ET USING STI44ET(11/84), INFRTIAL-BTI4NCZ, NB1060 DYN. DATA.

*
* * *
*********** 60 DYN. DATA. *********

************ SD 1385[15

MACHA OA (-)
1940
(DEG)
(DEG)
(0)
VELA (FOS)
ALTOF (FT)
TIME (SEC)

CEC. CET. CET. CET. CEC. CEG.											
Color Colo	2	+	ū	3	0	7 M	F T A	I	A C H		
C22 C23621.6 C2469.4 C-62.134 C-62.135 C-	SEC	11.	FPS	3.EG		OEG	(DEG	(DEG	£	(PSF)	1
1,22.0 236221.0 22409.9 -179 76.503 -62.133 -62.135 -62.147	6.00	36332	7428	6	6.48	2.13	~	9.20	3.92	0.70	
25610.3 22391.2 -177 76.525 -62.147 .055 39.174 23.869 30 226.0. 235610.3 22372.1 -177 76.566 -62.295 -001 39.176 23.814 31 2256.0 22352.1 -177 76.566 -62.295 -001 39.178 23.814 31 223.81	2000	3622	2409	1	6.50	62.13	2	9.18	3.89	0	
C26.0 286CU(.5 22372.1 -177 76.566 -62.275 001 39.178 23.841 31 C26.0 255691.6 22352.8 -175 76.566 -62.375 -041 39.178 23.881 31 C32.0 225675.5 22314.7 -175 76.607 -62.016 -011 38.824 23.788 31 C32.0 225566.2 22295.9 -174 76.607 -62.016 -011 38.824 23.799 31 C33.0 225566.2 22297.2 -174 76.604 -017 38.625 23.799 31 C40.0 225546.2 -174 76.604 -017 38.723 23.779 31 C40.0 225247.2 -174 76.604 -012 38.723 23.779 31 C40.0 225247.2 -174 76.604 -012 38.723 23.779 31 C40.0 225247.2 -174 76.607 -61.39 -62.479 23.471 <td< td=""><td>024.0</td><td>36110</td><td>2391</td><td>17</td><td>6.52</td><td>62.14</td><td>5</td><td>9.17</td><td>3.86</td><td>0.90</td><td></td></td<>	024.0	36110	2391	17	6.52	62.14	5	9.17	3.86	0.90	
235591.6 23952.8 -176 76.566 -62.375 -004 39.132 23.814 31 230.0 239783.3 -175 76.587 -62.017 -0014 38.874 23.759 31 234.0 235566.2 22233.7 -175 76.609 -017 38.875 23.731 31 235.0 23566.2 22257.2 -174 76.679 -01.719 -01.6 38.672 23.731 31 236.0 23564.2 22257.2 -174 76.671 -61.552 -023 38.676 23.731 31 236.0 23544.4 22236.4 -174 76.692 -61.391 -023 38.676 23.731 31 24.0 23544.4 22237.4 -174 76.692 -61.392 -023 38.762 33.731 31 24.0 23544.4 22237.4 -175 76.792 -61.392 -023 38.793 31 24.0 23546.2 236.2 -174 7	0.440	36636	2372	17	6.54	62.29	0	9.17	3.84	1.00	
030.0 235783.3 22314.7 175 76.587 -62.175 014 38.971 23.786 31 032.0 2356783.3 22214.7 175 76.607 -62.010 011 38.622 23.786 31 034.0 235646.2 22277.2 174 76.649 -01.719 016 38.662 23.734 31 036.0 23546.2 22277.2 174 76.671 -61.552 023 38.662 23.734 31 040.0 23547.4 22231.1 174 76.671 -61.552 023 38.662 23.734 31 042.0 23547.4 22231.1 174 76.671 -61.552 023 38.672 23.677 31 046.0 23547.4 22231.1 174 76.75 -60.895 023 38.672 23.677 31 046.0 23477.4 76.77 -60.895 023 38.670 23.657 31 046.0 23477.	0.000	35691.	2352	17	6.56	62.37	4	9.13	3.81	1.10	
1.35.u 255675.5 22214.7 175 76.607 -62.010 011 38.824 23.731 31.832.2 235675.2 23.731 38.723 23.731 31.832.2 23556.2 22255.6 174 76.671 -61.552 023 38.684 23.677 31.832.2 23.577.2 174 76.671 -61.552 023 38.684 23.677 31.832.2 23.677 31.832.2 23.677 31.832.2 23.677 31.832.2 23.677 31.832.2 23.677 31.832.2 23.677 31.832.2 31.832.2 23.677 31.832.2 31.832.	030.0	35783	2333	17	6.58	62.17	$\boldsymbol{\vdash}$	8.97	3.78	1.20	
0.34-0 2.35-66.2 2.2295.9 -174 76-649 -61.869 -0.01 38.723 23.731 31 0.34-0 2.35-66.2 2.2277.2 -174 76-649 -61.319 -0.02 38.662 23.734 31 0.40-0 2.35-61.2 2.2277.2 -174 76-671 -61.232 -66.62 23.734 31 0.40-0 2.35-61.2 2.2287.3 -174 76-692 -61.392 -62.4 38.662 23.704 31 0.42-0 2.35-61.3 -174 76-734 -61.232 -62.4 38.769 23.650 31 0.42-0 2.35-61.3 -174 76-776 -60.895 -03.9 38.769 23.650 31 0.44-0 2.35-61.3 -175 76-776 -60.895 -03.9 38.769 23.560 31 0.44-0 2.34-61.5 -175 76-376 -60.895 -03.9 38.779 23.560 31 23.560 31 23.560 31 23.560	032.0	35675	2314.	.17	6.60	62.01	-	8.82	3.75	1.29	
0.36.0 2.55461.2 2.2277.2 174 76.649 -01.719 016 38.662 23.704 31 0.36.0 2.35354.3 2.2258.6 174 76.671 -61.552 023 38.664 23.677 31 0.40.0 2.35140.7 2.2233.9 174 76.734 -61.232 024 38.669 23.659 31 0.40.0 2.35140.7 2.2221.1 174 76.734 -61.832 034 38.669 23.659 31 0.42.0 2.34620.2 2.2184.7 174 76.734 -61.865 033 38.769 23.596 31 0.46.0 2.34620.2 2.2184.7 175 76.776 -60.696 020 39.696 23.596 31 0.55.0 2.3460.5 2.2187.7 175 76.89 -60.417 -019 23.646 23.676 32.646 32.646 32.646 32.646 32.646 32.646 33.646 33.646 33.676 33.676 33.676	034.0	35566	2295	.17	6.62	61.86	0	8.72	3.73	1.39	
C35534.3 22258.6 174 76.671 -61.552 023 38.684 23.657 31 040.0 235247.4 22239.9 174 76.692 -61.331 024 38.713 23.650 31 042.0 235247.4 22502.4 174 76.734 -61.232 024 38.733 23.650 31 044.0 234927.1 22103.4 174 76.756 -60.895 033 38.769 23.596 31 046.0 234606.5 22164.7 174 76.776 -60.895 039 38.769 23.516 31 050.0 234713.4 22164.9 175 76.777 -60.417 020 39.068 23.516 32 052.0 234499.5 22108.4 175 76.818 -60.465 020 39.068 23.516 32 052.0 234499.5 22108.4 175 76.818 -60.465 020 39.026 23.549 32 <t< td=""><td>036.0</td><td>35461</td><td>2277</td><td>17</td><td>6.64</td><td>61.71</td><td>0</td><td>8.65</td><td>3.70</td><td>1.48</td><td></td></t<>	036.0	35461	2277	17	6.64	61.71	0	8.65	3.70	1.48	
046.0 235247.4 22239.9 -174 76.692 -61.391 -023 38.713 23.650 31 042.0 235140.7 22221.1 -174 76.713 -61.232 -024 38.690 23.623 31 044.0 235140.7 22221.1 -174 76.755 -60.895 -033 38.757 23.559 31 044.0 234927.1 22183.7 -174 76.755 -60.895 -033 38.794 23.596 31 046.0 234620.2 22164.7 -175 76.775 -60.564 -039 38.934 23.515 32 052.0 234499.5 22127.5 -175 76.817 -60.417 -011 39.079 23.498 32.052 31.498 052.0 234499.5 22127.5 -175 76.817 -60.465 -031 39.079 23.498 32.052 0.047 39.068 23.515 32.054 0.052 0.047 39.068 23.515 32.054 0.052 0.047 39.068 23.515 32.054 0.052 0.047 39.079 23.498 32.052 0.047 39.079 23.498 32.056 0.047 39.079 23.498 32.056 0.047 39.079 23.498 32.056 0.047 39.079 23.498 32.056 0.047 39.079 23.498 32.056 0.047 39.079 23.498 32.056 0.002 23.4175.9 22049.7 -018 39.408 23.513 32.049 32.056 0.002 23.499 0.002 23.	0383	35354	2258.	.17	6.67	61.55	8	8.68	3.67	1.58	:
042.0 235140.7 22221.1 -174 76.713 -61.232024 38.690 23.623 31	04040	35247	2239.	.17	69.9	61,39	2	8.71	3.65	1.68	4
044.0 235033.9 22202.4174 76.734 -61.065033 38.679 23.596 31 046.0 234927.1 22183.7174 76.755 -60.895033 38.769 23.569 31 048.0 23422.2 22164.7175 76.776 -60.564039 38.034 23.569 31 052.0 234506.5 22145.5175 76.817 -60.467011 39.079 23.515 32 052.0 234499.5 22108.4175 76.818 -60.465011 39.079 23.488 32 054.0 23422.2 22189.2175 76.818 -60.465011 39.079 23.488 32 055.0 234284.3 22069.5175 76.878 -60.465018 39.628 23.481 32 056.0 234284.3 22069.5176 76.878 -61.144 .025 39.528 23.495 32 056.0 234286.6 22089.7179 76.878 -61.438 .002 39.528 23.349 32 056.0 234286.1 221900.5184 76.956 -61.997025 39.528 23.349 32 056.0 233728.7 21971.2186 76.976 -62.377 -005 39.528 23.293 32 070.0 233496.3 21932.0191 76.996 -62.347 .033 39.778 23.293 33 072.0 233496.3 21932.0196 77.034 -62.347 .033 39.981 23.207 33 074.0 233366.6 21902.1200 77.034 -62.883 .043 40.263 23.179 33	045.0	35140.	2221.	.17	6.71	61.23	2	8.69	3.62	1.77	
046.0 234927.1 22183.7 -174 76.755 -60.895033 38.769 23.569 31	7 4 4 7	35033	2202	.17	6.73	61.06	.03	8.67	3.59	1.87	
048.0 234820.2 22164.7175 76.776 -60.564039 38.934 23.515 32 050.0 234606.5 22127.5175 76.797 -60.564020 39.068 23.515 32 32 052.0 234606.5 22127.5175 76.817 -60.417011 39.079 23.488 32 23.499.5 22108.4175 76.838 -60.465 .047 39.120 23.461 32 054.0 234.99.5 22089.2175 76.838 -60.465 .006 39.248 23.461 32 056.0 234.99.5 22089.2176 76.878 -60.979018 39.528 23.491 32 056.0 234.056.5 22089.7177 76.898 -61.144 .025 39.528 23.377 32 056.0 234.056.6 22029.8177 76.936 -61.144 .025 39.528 23.377 32 056.0 234.056.6 22029.8184 76.936 -61.997055 39.528 23.399 32 056.0 23.399.5 21937.0184 76.936 -61.997025 39.588 23.293 32 056.0 23.399.3 23.399.3 23.399	046.0	34927	2183.	.17	6.75	60.89	.03	8.76	3.56	1.97	1
052.0 234513.4 22145.5 -175 76.797 -60.564020 39.068 23.515 32 052.0 234606.5 22127.5 -175 76.817 -60.417011 39.079 23.488 32. 052.0 23469.5 22108.4 -175 76.838 -60.465 .047 39.120 23.488 32. 054.0 23499.5 22108.4 -175 76.838 -60.465 .047 39.120 23.481 32. 056.0 234284.3 22069.5 -177 76.878 -60.965 -018 39.248 23.49 32. 056.0 234175.9 22049.7 -178 76.898 -61.144 .025 39.528 23.349 32. 060.0 234175.9 22049.7 -181 76.936 -61.144 .025 39.528 23.349 32. 064.0 23406.6 22029.8 -181 76.936 -61.144 .025 39.528 23.349 32. 066.0 23428.7 21971.2 -184 76.936 -61.978 .006 39.525 23.259 33. 072.0 233490.3 21971.2 -191 76.996 -62.347 .033 39.778 23.259 33. 072.0 233490.3 21912.1 -200 77.035 -62.883 .045 40.265 23.179 33. 074.0 233286.6 21932.0 -205 77.052 -62.883 .043 40.263 23.179 33.	0.48.0	34870	2164.	.17	6.77	66.73	03	8.93	3.54	2.06	
052.0 234499.5 22127.5175 76.817 -60.417011 39.079 23.488 32.054.0 234499.5 22108.4175 76.838 -60.465 .047 39.120 23.461 32.054.0 234499.5 22108.4176 76.859 -60.707 .006 39.248 23.461 32.056.0 234284.3 22069.5177 76.878 -60.965018 39.408 23.405 32.056.0 234175.9 22049.7178 76.898 -61.144 .025 39.528 23.377 32.052.0 234175.9 22049.7178 76.917 -61.438 .002 39.528 23.377 32.052.0 234175.9 22049.7181 76.936 -61.997024 39.520 23.349 32.056.0 2342843.6 21990.5181 76.936 -61.997024 39.525 23.293 33.077 233239.5 21932.0191 76.996 -62.347 .033 39.778 23.293 33.0778 23.23239.5 21932.0196 77.034 -62.735 .033 39.778 23.2327 33.0778 23.23239.5 21871.8191 77.034 -62.735 .033 39.981 23.2327 23.149 33.0778 233239.5 21871.8206 77.034 -62.735 .033 233239.5 21871.8206 77.034 -62.735 .033 233239.5 21871.8209 77.034 -62.735 .033 233239.5 21871.8209 77.034 -62.735 .033 233239.5 21871.8209 77.034 -62.735 .033 233239.5 21871.8209 77.034 -62.883 .043 40.263 23.149 33.035 .043 40.256 23.119 33.035	050.0	34713	2145.	.17	6.79	60.56	•02	90.6	3.51	2.16	
U554.0 234499.5 22108.4 175 76.838 -60.465 .047 39.120 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 22.489 39.248 22.489 39.248 22.489 39.248 22.489 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 23.449 39.248 39.248 39.248 39.248 39.249	052.0	34606.	2127.	.17	6.81	60.41	.01	4.07	3.48	2.26	
0.56.0 234392.2 22089.2 -176 76.859 -60.707 .006 39.248 23.434 32.656 32.666.5 23.406 23.434 32.656 23.406 23.207 33.207 23.207	0.400	34499	2108.	.17	6.83	60.46	40	9.12	3.46	2.35	
C56.0 234284.3 22069.6 177 76.878 -60.965 018 39.408 23.405 33.405	0.940	34392	2689.	.17	6.35	60.70	00	9.24	3.43	2.45	
C60.0 234175.9 22049.7 178 76.898 -61.44 .002 39.528 23.349 32.0520 23.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.349 32.321	0.880	34284	2069.	.17	6.87	96.09	5	0.40	3.40	2.54	
C62.0 234066.6 22029.8 179 76.917 -61.438 .002 39.520 23.349 32 C64.0 233956.1 22410.0 181 76.936 -61.997 024 39.525 23.293 32 C66.0 233728.7 21971.2 184 76.956 -61.997 024 39.525 23.293 32 C68.0 233728.7 21971.2 186 76.976 -62.175 .006 39.568 23.265 33 C70.0 2.3511.0 21951.8 191 76.996 -62.347 .033 39.778 23.207 33 C72.0 233490.3 21937.0 196 77.015 -62.532 .039 39.978 23.207 33 C74.0 233366.6 21912.1 206 77.034 -62.715 .045 40.146 23.179 33 C76.0 233239.5 21892.0 209 77.070 -62.883 .043 40.263 23.149 33 C76.0 233239.5 21871.8 209 77.070 -62.035 <td< td=""><td>0.090</td><td>34175</td><td>2049.</td><td>17</td><td>68.9</td><td>61.14</td><td>2</td><td>9.52</td><td>3.37</td><td>5.64</td><td></td></td<>	0.090	34175	2049.	17	68.9	61.14	2	9.52	3.37	5.64	
0.64.0 233956.1 22010.0 181 76.936 -61.997 024 39.525 23.293 32 0.66.0 233843.6 21990.5 184 76.956 -61.997 024 39.525 23.293 32 0.68.0 233728.7 21971.2 186 76.976 -62.175 .006 39.568 23.265 33 0.70.0 2.3351.0 21951.8 191 76.996 -62.347 .033 39.778 23.236 33 072.0 2.33490.3 21932.0 196 77.015 -62.532 .039 39.981 23.207 33 074.0 233366.6 21912.1 200 77.034 -62.715 .045 40.146 23.178 33 074.0 233239.5 21892.6 205 77.070 -63.035 .063 40.265 23.149 33 0.78.0 233239.5 21871.8 209 77.070 -63.035 .065 40.256 23.119 33	0.62.0	34,066	2029.	.17	6.91	61.43	00	9.52	3.34	2.74	
66.0 233843.6 21990.5 184 76.956 -62.175 024 39.525 23.265 33 668.0 233728.7 21971.2 186 76.976 -62.175 .006 39.568 23.265 33 670.0 2.3511.0 21951.8 191 76.996 -62.347 .033 39.778 23.236 33 672.0 2.35490.3 21932.0 196 77.015 -62.532 .039 39.778 23.207 33 674.0 2333366.6 21912.1 200 77.034 -62.715 .045 40.146 23.176 33 675.0 233239.5 21892.0 205 77.052 -62.883 .043 40.263 23.149 33 675.0 77.07 -63.035 .051 40.256 23.119 33	0.000	33956.	2010.	1.0	6.93	61.78	05	9.51	3.32	2.84	
668.0 233728.7 21971.2 186 76.976 -62.347 .033 39.578 23.265 33 670.0 2.3511.0 21951.8 191 76.996 -62.347 .033 39.778 23.236 33 672.0 2.33490.3 21932.0 196 77.015 -62.532 .039 39.78 23.207 33 674.0 233366.6 21912.1 200 77.034 -62.715 .045 40.146 23.176 33 675.0 233239.5 21892.6 265 77.052 -62.883 .043 40.263 23.149 33 675.0 77.070 -63.035 .051 40.256 23.119 33	0,660	33843	1990	.18	6.95	61.99	• 02	9.52	3.29	5.94	
070.0 253511.0 21951.8 191 76.996 -62.532 039 39.778 23.207 33 072.0 734.0 734.0 77.015 -62.532 039 39.778 23.207 33 074.0 233366.6 21912.1 200 77.034 -62.715 045 40.146 23.176 33 074.0 233239.5 21892.0 205 77.052 -62.883 .043 40.263 23.149 33 0.78.0 73.00 77.070 -63.035 .051 40.256 23.119 33	0.68.0	33728	1971	.18	6.97	62.17	00	9.56	3.26	3.05	
072.0 733490.3 21937.0 196 77.015 -62.715 .039 39.981 23.207 33 074.0 233366.6 21912.1 200 77.034 -62.715 .045 40.146 23.176 33 076.0 233239.5 21892.6 205 77.052 -62.883 .043 40.263 23.149 33 0.78.0 233108.9 21871.8 209 77.070 -63.035 .051 40.256 23.119 33	0.020	33011	1951	.19	66.9	62.34	m	9.77	3.23	3.16	
074.0 23356.6 21912.1200 77.034 -62.715 .045 40.146 23.178 3 U.26.0 233239.5 21892.6205 77.052 -62.883 .043 40.263 23.149 3 U.26.0 233138.9 21871.8209 77.070 -63.035 .051 40.256 23.119 3	0.220	33490	1932	91	7.01	2.53	ന	9.08	3.20	3.28	
076.0 233239.5 21892.6265 77.052 -62.883 .043 40.263 23.149 3	0.74.0	33366	1912	20	7.03	2.71	4	0.14	3.17	3.40	
6.78.0 222108.9 21871.8209 77.070 -63.035 .051 40.256 23.119 3	0.46.0	33739	1892.	2 C	7.05	2.88	*	0.26	3.14	3.52	
	678-0	33108	1871.	20	7.07	3.03	5	0.25	3.11	3.65	

PAGE

O	(PSF)	33.788	3.92	4.07	4.22	4.38	4.55	4.72	00.4	5.08	5.27	5.46	5.66	5.86	6.05	6.25	6.45	6.64	6.83	7.02	7.21	7.39	7.57	7.75	7.93	8.10	8.28	8.45	8.63	8.81	8.99
AC	3	3.08	3.05	3.02	5.66	5.96	2.93	5.89	2.86	2.83	2.79	2.76	2.12	5.69	5.66	2.62	5.59	2.55	2.52	2.48	2.45	2.45	2.38	2.35	2.31	2.28	5.24	2.21	2.18	2	2.11
I	(DEG	0.22	0.22	0.30	64.0	0.57	0.49	0.40	0.37	0.35	0.31	0.14	9.88	9.68	9.52	0.40	0.40	9.41	6.39	9.38	9.36	9.35	9.35	9.35	9.36	9.36	9:36	9.37	9.38	39.380	• 36
T A	(DEG)	40	9	03	6	03	00	.03	90	.05	•14	.15	90	.08	•02	•03	90	• 05	01	•01	00.	• 05	0.00	5	0.	00.	• 05	•09	.07	067	10
GMA	(DEG)	63.17	63.29	63.41	63.53	63.52	63.24	63.05	62.76	62.20	61.62	60.49	58.87	57.61	56.47	55.82	55.40	54.93	54.51	54.34	54.23	54.16	54.31	54.76	55.17	55.63	56.19	56.66	57.05	-57.474	57.90
90	(010)	7.08	7.10	7.12	7.13	7.15	7.17	7.18	7.19	7.21	7.22	7.23	7.24	7.26	7.27	7.28	7.30	7.31	7,33	7.34	7.36	7.37	7.39	7.40	7.41	7.43	7.44	7.45	7.46		48
Z	(950)	.21	2	.22	.23	.23	.24	24	.25	.25	•26	9	•26	.26	•26	.26	.26	.26	.26	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25	.25	257
4	(FPS)	1351.	1031.	1311.	1796.	1769.	1749.	1727.	1706.	1684.	1662.	1640.	1619.	1597.	1575.	1553.	1531.	1509.	1486.	1464.	1441.	1419.	1396.	1373.	1350.	1327.	1304.	1291.	1257.	1233.	21210.1
-	(FT)	32974.	32836.	32693	32546.	32395	32239.	32079.	31916.	31748	31577	31404	31224.	31053.	30878	30703	36525	30357.	30187.	30018	29851.	29686	29523	29361.	29230	29040	28880.	2872C.	28550	28397	228234.5
E	(SEC)	0.80	182	3 4 C	680	088	900	.92.	960	900	C98.	100.	102.	11.4.	106.	8077	110.	112.	114.	116.	118.	120.	122.	124.	126.	128.	130	332	124.	36.	1138.0



TIME (SEC)	ALTDE (FT)	VELA (FPS)	GAMA (DEG)	HDGA (DEG)	SIGMAA (DEG)	BETAA (Dēg)	ALPHAA (DEG)	MACHA	OA (PSF)	
	, de c	13.00	26	7.49	8.29	.14	0.14	2.07	9.18	
, o	27631	1161.	9 6	7.50	8.57	~	9.89	2.03	9.36	
146	27731.	1136.	25	7.51	8.96	.08	0.20	2.00	9.55	:
144	77559.	1112.	.27	7.51	9.39	01	8.82	1.96	9.75	
0.04	227332.8	21049.1	276	77.527	-54.782	129	38.989	21.930	39.957	
150	27231.	1065.	2	7.53	8.91	4	90.6	1.89	0.17	į,
15.	27016.	1041.	• 29	7.54	0.23	-	9.20	1.85	0.39	
154	7682b.	1017.	62.	7.55	0.01	.08	9.64	1.82	0.62	:
5	26631	0991.	3	7.55	9.47	7	0.11	1.78	0.85	
- 55 B	26432	9965	30	7.56	6.07	.10	0.24	1.74	1.09	
160	26230	0630	.31	7.56	6.79	60.	0.20	1.70	1.33	
162	26023	0913	31	7.57	5.51	.05	6.08	1.66	1.58	
404	25824	J887.	18	7.58	4.47	10	96.6	1.62	1.82	
9	25621.	0860.	.31	7.59	3.80	000	9.87	1.58	2.07	
6.8	25418	0834.	31	7.59	3.14	10	9.83	1.54	2.32	
70.	25217	3807.	.31	7.60	2.71	0	06.6	1.50	2.57	
72.	25016.	0781.	.31	7.61	2.46	08	46.6	1.46	2.81	
74.	24817	.753.	30	7.62	2.57	~	9.92	1.42	3.05	
76.	24620	0725.	.30	7.63	2.71	60	9.91	1.38	3.29	
8	24423	3698	.30	7.64	2.95	07	9.91	1.34	3.53	;
80.	24227	0671.	30	7.64	3.22	O	06.6	1.30	3.769	
8 2	24031.	0644.	.30	7.65	53.58	~	9.92	1.26	4.006	
4	23835.	0616.	.30	7.60	3.96	0	9.92	1.22	4.242	
186	23639.	U588.	.30	7.66	4.35	4	8.95	1.18	4.478	
000	23443	0560	.30	7.66	4.55	8	16.6	1.14	4.714	
300	23247	0531.	.31	7.67	54.64	•	9.85	1:10	4.952	PA OL
192	23049	3503.	.31	7.67	4.71	0	9.84	1.06	5.191	
194	22851.	0474.	.31	7.67	54.93	8	9.85	1.02	5.431	
196	22621.	3445	3	7.57	5.09	3	9.81	0.97	5.673	
							•	,	, ,	

O	(PSF)	46.164	6.41	99.9	6.91	7.16	7.41	7.66	7.91	8.16	8.40	8.64	8.87	60.6	9.31	9.53	9.74	9.04	0.15	0.35	0.55	0.75	0.95	1.15	1.35	1.56	1.77	1.98	2.19	2.40	2.61	
Ċ	<u> </u>	8	0.85	0.81	0.76	0.72	0.68	99.0	0.59	0.55	0.51	0.47	0.42	0.38	0.34	0.29	0.25	0.21	0.17	0.12	0.08	0.04	66.6	9.95	0.01	9.86	9.85	9.77	9.73	9.68	49.6	
V H d		.61	9.65	9.71	9.68	9.53	39.388	9.28	9.16	9.08	90.6	90.6	9.04	9.02	0.03	4.07	60.6	90.6	9.10	9.11	9.13	9.10	4.07	9.30	8.93	8.95	8.98	8.97	8.97	60.6	9.16	
7	(DEC)	40	00	•0•	.07	•07	092	.10	• 03	6	60	07	9	21	19	18	18	17	13	12	07	12	05	3	03	0	04	10	18	5	0	
IGMA	(DEG)	55.21	55.20	55.12	54.76	54.21	-53.663	52.99	52.20	51.53	51.18	51.03	50.93	50.99	51.27	51.71	52.27	52.88	53.34	53.77	54.02	54.24	54.60	54.60	54.39	54.11	53.90	53.67	53.63	53.91	54.27	
90	(DEG)	67	7.67	7.67	7.67	7.67	77.673	7.67	7.66	7.65	7.66	7.66	7.65	7.65	7.64	7.64	7.63	7.62	7.61	7.60	7.59	7.58	7.56	7.55	7.53	7.51	7.50	7.48	7.47	7.45	7.43	
A	(DEG)	.31	32	• 32	.32	.32	2	.32	.32	.32	.31	.31	.31	30	.30	30	.30	•29	.29	.29	.30	.30	.30	.30	.30	•30	.31	.31	.31	.31	317	
	(FoS)	0387.	0356	J328	3298	J268.	3238°	J208.	o177.	J147.	0116	0085	0054.	3623	369E	1966.	1928	9886	9864.	9832.	4799.	3766.	¥732.	369£	9645.	9632.	9598.	4565	9531.	9497	13462.7	
_	(FT)	22230.	22047	71643	21638.	21432	21227	21023	20819.	20617.	20418	20220	20026.	19834	19645	19459	19274.	19090	18908.	18725.	18543.	1836C.	18170.	17992	17807.	17621.	17434.	17246.	17057	16867	210677.2	
1	(SEC)	200	000	707	206	o. 0 /	216.	212.	214.	216.	21.5	220.	222	224.	126.	228	730.	232.	234.	136	7.38	.46	242	744	46.	748	25.6.	252	254	256.	1258.0	

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OF	POOR	QUALI	TY

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3 .	_	<u>ب</u>	X V	9	A E	V V	r L	و ا ا	
(SEC)	(FT)	(FPS)	(930)	(0EG)	(066)	(066)	(066)		(45d)
260.	16485	442 A.	.32	7.41	4.68	9	9.13	9.59	52,823
262	10.04	9393	~	7.39	5.05	4	9.11	9.55	3.03
1000	1004	25.00		7.37	5.40	0	9,13	9.50	3.25
26.1	- XOX -	0222	1 (4	7 . 34	5.64	-	9.18	9.46	3.48
0 4 0 4 0 5	15406	0000	9 (6	7.32	5.73	~	9.25	9.41	3.70
200	15421	9252	t	7.29	55.77	m	9.30	9.37	3.94
040	10044	0216.		7.27	5.76	m	9.37	9.32	4.18
274.	10071	0180	1	7.24	5.69	~	9.43	9.27	4.43
276.	14854	0142	· ·C	7.21	5.66	8	9.51	9.22	4.68
- X	14625	9105	3 6	7.18	5.76	4	9.62	9.18	4.94
2000	14411	9068	37	7.15	55.85	01	9.66	9.13	5.21
7 20 7	14155	9031	80	7.12	5.91	-	9.61	9.08	5.48
79.4	13954	3993	3	7.09	55.86	m	9.61	9.03	5.76
280	13720.	3955	• 39	7.05	5.85	90	9.65	8.98	6.05
288	13482	4917.	04.	7.02	6.02	10	69.6	8.93	6.35
000	13246.	8879	3	6.98	3.04	Ó	9.16	8.88	99.9
202	12997	8841.	4.0	6.96	1.08	25	9.76	8.83	96.9
704	12756	3802	40	6.92	2.55	38	9.62	8.78	7.26
206.	12514	8763.	40	6.89	1.04	. 45	9.68	8.73	7.57
208	12274	8724	40	6.86	0.31	13	0.50	8.68	7.86
0.0000	212038.3	13682.2	397	76.827	-49.942	050	40.782	18.629	8.13
30%	11807	8640	39	6.79	9.63	40	0.29	8.57	8.39
304	11540	8598	.38	6.75	64.6	02	0.02	8.52	8.64
306	11359	3558	37	6.71	0.18	02	9.77	8.47	8.89
3 C C C C C C C C C C C C C C C C C C C	11162	8517	37	6.68	1.36	05	9.58	8.42	9.13
9 7 6	10926	8477	2	49.9	2.80	0	9.43	8.37	9.37
312	10710	8437	37	6.60	4.30	02	9.39	8.32	9.61
216.	10493	B 397	3	6.55	5.85	4	9.41	8.27	9.85
216.	10271	8357.	3	6.50	6.97	00	9.45	8.22	0.10
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OA (PSF)	60.639	3 2 5	7 2 2 2	000		2.62	29.2	3.00	3.41	3.82	4.24	4.67	5.35	5.81	6.27	6.74	7.21	7 7			0 0	40.0	9.48	9.91	0.34	0.77	1.19	1.62	2.04	2.50		,
4ACHA	18,123	3.0	300	96.	1691	1.86	7.80	7.75	69.1	7.64	7.58	7.53	7.50	7.45	7.30	75 6		000		7107	1.12	7.06	7.01	6.05	9.90	6.84	6.79	6.73	6.67	K . K	70.0	0.0
ALPHAA (DEG)	39.536	. 62		. 77	. 81	. 89	83	. 79	. 81	85	9.85	9.85	0.01	6	4	•			700	63	9.64	9.64	9.65	9.65	9.65	9.64	9.6	74.0	6		0	
BETAA (DEG)	_		.14	.16	5	4	.21	3	.16	.17		16				77.	5	2	4	=	7	14	E =	5	10	80	6		5		J	_
SIGMAA (DEG)	58.0	-58.442	99.89	96.76	8.72	58.62	3.29	7.66	57.08	56.78	56.50		40.40	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		00.00	54.15	53,58	53.25	53.00	53.05	53.37	53.79	54.27	34.76	55.14	, ת י יי			16.00	56.60	56.73
HD GA (DEG)	64.0	76.352	5.29	.5.0	5.13	5.12		56.5	5 . 33		. a	20.4	•		0 a	2.78	5.72	99.5	5.29	5.53	5.47	5.40	5 34	5.27			7 7 7	5 6		4 • 3	4 • 8 ·	4.7
6 4 M A () E G)	4 1	424	43	45	45	47	. 4		, r	4 6	, n	7	i G		2	4	35	55	25	10 2	5.4	5.4	, L	, R	7 4		ָר י	ָרְ וּיִי	,	C.	56	5.
VFLA (FPS)	3276.	3235	7018	1152	1110		0000	0000	0000	• 0 • 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0 · 0	3000	/ K 7 C •	7808	7797.	7754.	7711.	7668.	7625.	7581.	7538	7607	0774				, 31 4. - 2 2 4 4	120%	7222	7175.	7127	7083.	17036.7
ALTOE (FT)	0.000	5.550		1400c			000000	• 10000	11700.	0,000	07378•	. 7677	06772.	06404.	06153.	05840	05526.	05213	00000	0 F 3 30	00000	3000		03072	03370	C3C58•	02767.	02466.	02164.	01860.	01554	201246.7
TIME (SEC)	000	200		964	0.000	9000	3.00	. 750	334	336.	3.3.R.	340.	342.	344.	346.	348	350.	352	777	- 4	• • • • • • • •	• 0 0 0	300	306	364.	366.	368.	370.	372.	374.	276	1378.0

ST14BET USING ST14MET(11/94), INERTIAL-BT14NO2, NB1060 DYN. DATA.

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Check Chec	(0FG) (0FG)	(DEG) BBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBBB	14.007 14.007 14.007 14.007	00.339 90.339 90.339 91.338 91.795 93.757 94.095
190039.2 15335.5756 71.151 -53.84 189237.7 15212.0748 70.724 -55.14 18932.0 15149.5747 70.724 -55.14 183232.0 15149.5747 70.724 -55.14 183232.0 15149.5747 70.724 -55.14 182374.3 14956.7748 70.620 -56.69 18744.0 14827.0775 70.098 -58.23 186371.5 14696.6771 69.933 -58.23 18524.3 14493.2807 69.249 -57.61 185237.5 14264.9822 69.090 -54.99 18475.7 14359.8821 69.249 -57.61 18475.7 14359.8821 69.249 -57.61 182224.3 14266.2807 68.299 -54.99 183174.5 14098.7754 68.011 -47.679 182377.5 14098.7617 67.823 -46.70 182337.5 13970.9550 67.551 -29.52 16.207.5 13644.2550 67.551 -29.52 16.207.5 13644.2550 67.551 -29.52 16.207.5 13644.2550 67.551 -29.52 16.207.5 13644.2550 67.551 -29.52 16.207.5 13644.2550 67.551 -29.92 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 13644.2550 67.551 -29.52 12.207.5 12.20		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	3 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	21.000 21.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.000 20.0000 20.000 20.000 20.0000 20.000 20.000 20.000 20.000 20.000 20.0000 20.
189650.5 15274.0 -752 71.011 -54.24 189650.5 15274.0 -748 70.724 -55.14 189237.0 15149.5 -748 70.724 -55.14 189237.0 151272.0 -748 70.574 -55.14 188236.0 15021.0 -748 70.574 -55.14 187236.1 -778 70.574 -55.14 18724.0 15021.0 -778 70.693 -56.69 18774.0 14751.7 -778 70.093 -58.02 18774.0 14751.7 -778 69.596 -58.02 185371.5 14631.2 -781 69.693 -58.02 185224.3 14426.2 -780 69.596 -58.86 185224.3 14426.2 -780 69.596 -58.86 185224.3 14426.2 -780 69.249 -57.61 185228.6 -780 69.249 -57.61 183787.8 14228.6 -7843 69.090 -54.95 183787.8 14034.6 -751 69.143 -46.70 182174.5 14034.6 -751 69.143 -46.70 182174.5 13977.1 -550 67.556 -29.52 182174.5 13544.2 -751 69.00 69.00 69.00 182174.5 13644.2 -751 69.00 69.	448888899944		44444444 4444444 444444 444	4 4 3 3 3 3 3 4 4 4 4 4 4 4 4 4 4 4 4 4
1862977 15212.0 -748 70.669 -54.64 184932.0 15212.0 -746 70.574 -55.82 185206.6 15081.0 -746 70.574 -55.82 186206.6 15081.0 -746 70.574 -55.82 18744.3 14956.7 -772 69.933 -58.23 18714.0 14827.0 -772 69.933 -58.23 18714.0 14827.0 -772 69.933 -58.28 69.24 18524.3 14631.2 -773 69.596 -59.86 18524.3 14493.2 -807 69.249 -57.61 18524.3 14228.6 -807 69.249 -57.61 184475.7 14359.8 -7808 68.924 -57.49 182277 14359.8 -7808 68.299 -46.79 182277 14098.7 -685 68.299 -46.79 182277 14098.7 -685 68.299 -46.70 182277 13970.9 -550 67.571 -39.10 182174.5 13977.1 -550 67.551 -39.10 182174.5 13977.1 -59.9		00000000000000000000000000000000000000	4444444 444444 0000000000000000000000	4 E O W U U U U U U U U U U U U U U U U U U
18922.0 15149.5747 70.72455.14 16932.0 15149.5746 70.57455.14 16950.c 6 15084.8748 70.57455.14 16350.c 6 15021.0748 70.57455.14 16723.6 15021.0754 70.09856.69 16714.0 14827.0752 70.09858.23 16714.0 14827.0720 69.09358.23 16751.5 14695.5807 69.09057.61 18524.3 14493.2821 69.09054.35 16524.3 14493.2821 69.09054.35 1675.7 14359.8720 68.45647.49 1837471.8 14228.6720 68.45647.49 182174.5 14034.6635 68.29946.70 18228.5 14034.6631 68.14346.70 182387.7 13970.9550 67.55139.10 162176.5 135471.7 67.55629.52 16.2176.5 13547.2550 67.55139.10			444444 0000000000000000000000000000000	44 may 2 may
166500.6 15084.8 -746 70.574 -55.82 16820.6 15021.0 -746 70.524 -55.82 18744.3 14956.7 -754 70.261 -57.53 18744.3 14956.7 -752 70.098 -58.02 187714.0 14827.0 -771 69.933 -58.23 186371.5 14696.6 -793 69.596 -58.86 18524.3 14693.2 -807 69.249 -57.61 185224.3 14493.2 -822 69.249 -57.67 18475.7 14264.9 -784 68.765 -48.91 184475.7 14264.1 -784 68.765 -48.91 184475.7 14264.1 -784 68.765 -48.91 1828377.8 14163.4 -68.5 68.456 -47.49 182835.6 13970.9 -51.7 67.985 -46.70 182835.6 13970.9 -550 67.551 -39.10 182377.7 13977.1 -550 67.556 -20.03		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4444 9444	44.000.49
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187244.3 14956.7754 70.261 -57.53 187644.3 14956.7754 70.098 -58.23 187644.5 14891.9771 69.933 -58.23 187644.6 14761.7731 69.933 -58.23 186371.5 14696.6793 69.596 -58.45 18550.9.6 14564.9793 69.596 -58.86 184475.7 14256.2821 69.090 -54.35 164644.4 14426.2821 69.090 -54.35 184475.7 14359.8754 68.924 -57.61 184475.7 14359.8754 68.924 -57.61 183471.6 14163.4754 68.14347.07 182633.6 13970.9589 67.82346.76 182337.7 13907.1550 67.556 -29.52 16.2176.5 13644.251.46 70.033	34 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.21 4.01 4.00 3.93	4.00
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186371.5 14627.0771 69.933 -58.23 186371.5 14696.5793 69.596 -58.645 185593.5 14631.2807 69.090 -54.35 155524.3 14493.2822 69.090 -54.35 16444.4 14426.2807 69.090 -54.35 164475.7 14359.8784 68.924 -51.46 184475.7 14359.8784 68.011 -47.49 183174.5 14098.7617 67.985 -46.70 182235.6 13970.9589 67.823 -46.70 182337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 13907.1550 67.556 -29.50 18.2337.7 1350.7 1550 67.556 -29.50 18.23 67.556	34.00	9.50	4.07 4.00 3.93 3.87	4.09
186371.5 14696.6 -793 69.596 -58.45 186371.5 14696.6 -793 69.596 -58.86 1855.24.3 14631.2 -822 69.249 -57.61 182377.7 13977.1 -55.0 67.65 -48.91 18233.6 14034.6 -617 67.945 -46.76 18233.6 139770.9 -55.0 67.55 -70.03	.06 11 37	04.0	4.00 3.93	4.09
186371.5 14696.6793 69.596 -58.86 186371.5 14691.2807 69.69.69.24 -59.20 185524.3 14493.2822 69.249 -57.61 185224.4 14426.2822 69.090 -54.35 184475.7 14294.1784 68.91 -47.49 182377.7 13970.9589 67.823 -46.70 182337.7 13970.9589 67.823 -46.70 182337.7 13977.1550 67.556 -29.52	11.	6.40	3.93	4.57
165943.5 14631.2807 69.424 -59.20 16524.3 14493.2822 69.249 -57.61 165224.3 14493.2822 69.249 -57.61 164644.4 14426.2808 68.924 -51.46 184475.7 14359.8784 68.765 -48.91 184122.7 14228.6724 68.011 -47.49 183787.8 14163.4685 68.299 -46.70 182235.6 14034.6617 67.985 -46.70 182387.7 13907.1550 67.556 -29.50 10.0	.37		3.87	7.7
16560.9 t 14564.9	.37	9.52		0000
165224.3 14493.2 -821 69.090 -54.35 164644.4 14426.2 -808 68.924 -51.46 184475.7 14359.8 -754 68.010 -47.49 184122.7 14294.1 -754 68.011 -47.49 183787.8 14228.6635 68.456 -47.67 182235.6 14034.6635 68.143 -46.79 182235.6 13970.9589 67.823 -46.70 182337.7 13907.1550 67.556 -29.52		9.59	3.80	5.57
164644.4 14426.2808 68.924 -51.46 18475.7 14359.8784 68.765 -48.91 184122.7 14204.1754 68.011 -47.49 183787.8 14228.6685 68.456 -47.67 182035.6 14034.6617 67.985 -46.76 182235.6 13970.9589 67.823 -46.70 182337.7 13907.1550 67.556 -29.52	.03	9.60	3.72	6.00
184475.7 14359.8784 68.765 -48.91 184122.7 14204.1754 68.011 -47.49 183787.8 14228.6720 68.456 -47.07 183471.6 14163.4685 68.299 -46.79 182835.6 14034.6617 67.985 -46.76 162633.6 13970.9589 67.823 -46.70 182337.7 13907.1550 67.556 -29.52	.16	9.54	3.65	9.49
184122.7 14294.1754 68.451 -47.49 183787.8 14228.6720 68.456 -47.67 183471.6 14163.4685 68.299 -46.79 183174.5 14098.7651 68.143 -46.70 182035.6 14034.6617 67.985 -46.70 18233.6 13970.9589 67.823 -46.70 182337.7 13907.1550 67.571 -39.10	.01	9.43	3.58	6.92
183787.8 14228.6720 68.456 -47.07 183471.6 14163.4685 68.299 -46.79 182835.6 14034.6617 67.985 -46.70 162633.6 13970.9589 67.823 -46.70 162170.5 13964.2477 67.556 -29.52	00	9.29	3.52	7.32
183471.6 14163.4685 68.299 -46.79 182835.6 14034.6617 67.985 -46.76 162633.6 13970.9589 67.823 -46.70 182387.7 13907.1550 67.571 -39.10	03	9.22	3.45	7.64
182075.6 14098.7617 68.143 -46.60 182075.6 14034.6617 67.985 -46.70 162633.6 13970.9589 67.823 -46.70 182387.7 13907.1550 67.571 -39.10 162170.5 13544.2477 67.556 -29.52	.03	9.15	3.38	7.90
18233.6 14034.6617 67.985 -46.76 162633.6 13970.9589 67.823 -46.70 182387.7 13907.1550 67.571 -39.10 162170.5 13544.2477 67.556 -29.52	10	9.03	3.32	8.10
162633.6 13970.9589 67.823 -46.70 162387.7 13907.1550 67.571 -39.10 162170.5 13544.2477 67.556 -29.52	S	8.95	3.26	8.23
182387.7 13907.1550 67.671 -39.10 18217C.5 13644.2477 67.556 -29.52	57	8.97	3.19	8.31
16217C.5 13844.2477 67.556 -29.52	•29	60.6	3.13	8.32
101000 A 112720 A 12880 A 1288	.08	00.6	3.07	8.23
	18	9.03	3.00	7.96
181872.2 13718.0267 67.463 -1C.30	26	9.03	2.95	7.55
364-1 104-104 A 114-104 C 14-104 C 14-1	15	9.05	2.88	6.86
181706.4 12580.5 - 020 181706.4 12580.5 - 020	4	9.01	2.82	9.00
121 121 121 121 121 121 121 121 121 121	.22	9.06	2.76	5.10
15.024 7 12442.4 .154 67.874 20.95	0	9.22	2.70	4.21

																														C	F	P.
G	(PSF)	3,3	2.45	1.58	0.72	9.88	.03	8.19	7.35	6.49	5.62	4.88	5.00	5.23	5.54	5.89	6.59	5.70	7.11	7.56	7.97	3.39	3.82	7.57	9.68).12	5.8	00.1	1.51	2.017	486	
AC	.	2.64	2.58	2.52	2.46	2.41	12,353	2.29	2.23	2.17	2,11	2.05	1.99	1.92	1.86	1.80	1.73	1.67	6.1	1.55	1.48	1.42	1.36	1.29	1.22	1.16	60.1	1.02	.95	.88	.82	
PHA	(DEC)	9.38	9.56	9.80	0.02	0.11	40.346	0.67	1.09	1.59	1.79	2.09	2.15	2,13	2.04	1.90	1.77	1.67	1.54	1.50	1.43	1.17	1.18	1.68	1.72	1.22	1.08	96.	81	09.0	07.0	
TA	(DEG)	•19	17	.12	25	18	.022	2	8	9	12	7	12	4	•08	5	.15	.18	.16	• 50	.17	• 36	20	•16	.11	4	.11	9	8	9	9	
GMA	(DEG)	0.14	0.36	0.59	44.5	2.72	74.460	5.41	5.56	5.34	3.88	0.62	6.24	26.0	7.09	4.28	1.23	9.58	8.51	8 . 88	1.57	0,38	2,01	2.32	2.71	2.96	3,32	3,53	8.89	3.29	5.71	
90	(DEC)	8.05	8.35	8.64	8.96	9.26	69.617	6.64	0.27	0.61	0.95	1.29	1.61	1,93	2.24	2.53	2.82	3.10	3.37	3.62	3.91	. 13	4.49	. 78	0.10	0.41	. 73	0.02	39	59.0	96.0	
AMA	(950)		23	20	(M)	8	083	200	.32	• 45	13.	68	.78	85	80	.93	65.	96	.97	.97	96	1.00	1.02	1.04	1.06	1.09	1.11	1.14	1.17	7.5	1.11	
VEL	(FPS)	3399	3336.	3273.	3211.	3149.	13087.5	3025.	2963.	2894.	2834.	2770.	2706.	2643.	2580.	2516.	2453.	2390.	2326.	2266.	2202	2137.	2073.	2008	93 H.	869.	801.	.727.	657.	587.	518.	
LT	~	82042.	82177.	R2309.	8541E.	62485.	182502.0	82454.	82371.	82223.	82017.	81760.	81428.	81120.	80759.	80331.	19992.	74538.	79201.	78835.	76407.	18004.	17595.	77179.	16750.	76326.	75836.	5441.	74934.	14526.	14036.	
E	(SEC)	500	502	504.	506.	508.	1510.0	512.	. 476	516.	118	520.	525	524.	526.	52ª.	530.	532.	534.	536.	38.	540.	545.	. 440	.940	.849	550.	52.	54.	56.	58.	

(PSF)	92.892	3.50	3.74	3.87	4.06	4.23	4.41	4.58	4.77	4.96	5.18	5.40	2.64	5.00	6.20	6.54	6.92	7.37	7.85	8.35	8.86	9.43	9.87	00.27	00.61	00.86	01.03	1.15	01.23	
4ACHA	10.758 10.693	0.62	0.56	0.49	0.43	0.37	0.30	0.24	0.18	0.12	0.06	0.00	9.64	• 88	.83	.77	.72	• 66	.61	.55	.50	• 45	04.	.35	• 50	.24	.19	.13	.08	
ALPHAA (DEG)	39.951	69.6	9.61	0.50	04.6	9.33	9.28	9.15	9.05	8.90	8.79	8.76	8.74	8.72	8.70	8.69	8.67	8.74	8.78	8.75	8.70	8.57	8.45	8.30	8.16	8.06	7.94	7.73	7.53	
BETAA (DEG)	-330	40.	00	90	Ę	16	17	7	16	14	60	90	11	10	90	08	10	7 4	H	18	15	16	12	07	10	40	07	02	10	
SIGHAA (DEG)	30.188 38.639	1.64	3.62	5.27	99.9	7.71	8.31	9.41	8.42	8.21	8.06	8.67	9.78	47.0	1.53	2.32	2.99	2.04	8.19	5.45	2.76	0.86	9.35	8.56	8.19	5.58	9.11	9.64	9.80	
HDGA (DEG)	77.235	7.81	8.12	ĕ.43	8.82	9.16	9.52	9.87	0.23	0.59	96.0	1.30	1.66	2.03	2.41	2.79	3.17	3.56	3.93	4.29	4.64	4.99	5,31	5.51	5.92	6.22	6.52	6.82	7.13	
6 A M A (0 F G)	-1.066	00	25.	96.	9.0	95	96.	.97	.97	90	66.	66	1.01	1.03	1.06	1.09	.12	1.16	1.18	1.19	1.16	1.16	1.13	1.10	1.07	1.04	1.01	96	96.	
VELA (FPS)	11450.3	1314	1247	1175.	1108.	1041.	0974.	090P.	3842.	0777.	0713.	.650.	0587	0525	3454.	0402	J342.	0282.	.0223	1163.	0105.	0051	9993	935.	877.	819.	761.	763.	646.	
ALTEE (FT)	173655.6	72836	72507	72142.	71781.	71423.	71065	7070F	70350	69991	69632.	69277	9000 a	6c542	68167	67735	67391.	66936	56571.	60154.	65740	6533	64935	64551	64179	63821	63474	63140	62815.	
TIME (SEC)	1560.0		10 C	500	570.	572.	574.	576.	F 7 C	20 20 20 20 20 20 20 20 20 20 20 20 20 2	7.00		7 10		000	502	294	20.0	508	6000	602	404	600	800	019	612	4 7 7		, 12 	

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6 E 28	0A (PSF)	01.32	01.39	101.38	01.35	01.31	01.29	01.27	01.26	01.27	01.30	01.34	01.37	01.48	51.68	01.93	32.23	02,56	03.01	3.54	34.05	34.78	5.55	36.32	01.09	7.84	8.58	39.25	9.87	10.43	0.95
V d ****	MACHA	• 02	6.	8.923	.86	.81	.78	.70	• 65	• 60	.54	449	.43	333	32	.27	21	.16	10	.05	66	93	88	83	77	.72	67	62	57	52	47
***	ALPHAA (DEG)	7.41	7.34	37.279	7.15	7.02	6.71	6.67	6.65	6.62	6.59	6.56	6.57	6.45	6.3¤	6.33	7.06	6.61	5.21	5.03	5.85	5.87	5 • 6E	5.51	5.44	5.29	5.14	. 90	4.63	4 4 4	• • 1 B
• DATA.	BETAA (DEG)	•16	11.	136	.17	• 10	~	8	ŏ	0	02	60	11	47	0	'n	01	0	60	08	55	34	21	\mathbf{a}	\circ	.21	\sim	• 33	.37	_	\sim
N81060 DYN	SIGMAA (DEG)		1.86	43.420	4.35	4.98	5.45	6.05	6.53	999	6.92	7.29	0.05	2,91	1.47	3.12	3.04	3.17	3.46	3.59	3.17	5.68	0.30	3.47	5.66	5.29	4.71	3.89	3.43	3.63	69.
L-8114N02,	HDGA (DEG)	7.43	7.71	88.034	8.36	8.69	9.02	9.35	9.70	40.0	0.39	0.73	1.05	1.42	1.79	2.17	2.56	2.96	3.37	3.78	+ . 22	4.52	4.98	5.32	5.66	96.6	30	. 62	96.0	1.27	.61
4 + + + + + + + + + + + + + + + + + + +	GAMA (JEG)	40.	.02	923	95	60.	40.	•	96.	1,61	1.04	1.07	1.10	1.17	1.24	.31	1.38	1.46	1.53	1.62	1.71	1.78	1.79	1.79	1.79	1.77	1.74	1.71	1.68	6.5	1.62
4467 (11/9. ******	VFLA (FPS)	590.	530.	3478.5	420.	363.	305.	243.	191	133.	075.	017.	95 A.	669	941.	783.	724.	552.	532.	545.	478.	119.	360.	505.	244.	186.	131.	374.	117.	961.	. 506
######################################	ALTGE (FT)	62435	62190.	161635.5	61532.	61279.	60974.	60 t 55.	60351.	60032.	597UE.	59371.	5902H.	50672.	58295	57931.	57485.	57050.	50595.	56118.	55619.	55637.	54566.	54040.	53510.	53030.	52493.	51997.	51513.	51042.	50582.
ST148ET	TIME (SEC)	620.0	622.0	1624.0	0.920	626.0	0.0€9	632.0	634.3	636.0	D38.∪	0.349	042.0	0.440	646.0	648.0	650.0	552.0	54.0	656.0	658.0	0.000	662.0	64.0	266.6	568.0	570.0	572.0	574.0	2.92	. 18.0

Q Q	(PSF)	11.43	11.87	12.32	12.75	13.18	13.60	14.04	14.51	14.96	15.32	15.55	15.69	15.71	15.55	15.30	15.02	14.82	114.753	14.79	14.98	15.29	15.72	16.28	16.95	17.72	18.58	10.45	20.45	21.46	22.49
AC	1	.42	.37	.32	.27	.22	114	.12	.07	.03	96.	.93	88	. R.4	.79	.74	.70	•65	6.611	•56	.52	• 48	•43	39	.35	.31	5.5	25	.18	14	10
₽ H d	(050)	3.90	3.66	3.26	3.16	3.10	3.00	2.86	2.82	2.83	2.65	2.42	2.07	2.04	1.99	1.84	1.56	1.21	31.390	1.14	1.14	1.03	0.95	0.85	0.74	0.63	0.51	0.34	0.18	0.01	9.77
TA	(DFG)	.16	01	40	98	10	13	13	57	07	03	I	15	0	05	05	•00	27	095	0	.11	.10	•00	0	• 07	.10	•08	•03	•04	\sim	•13
GFA	(0f3)	6.01	647	8.69	0.02	1.3E	2.33	2.87	40.0	9.28	9.50	9.58	8.5	11.50	22.26	32.97	43.45	48.64	-51,139	53.18	54.61	53.49	52.56	51.01	49.29	47.42	45.21	43.32	42.11	1.03	39.65
90	(DEG)	7.96	8.32	8.71	9.10	9.51	60.0	60.30	62.00	01.16	01.45	01.66	01.75	61.15	01.64	01.42	01.12	00.75	100.375	79.69	9.57	9.16	8.75	8.33	7.92	7.52	7.12	6.73	6.34	5.95	5.58
¥	(076)	1.59	1.58	1.57	1.58		1.61	1.64	1.66	1.64	1.57	1.47	1.36	1.25	1.16	1.11	1.12	1.20	1.3	1.43	1.56	1.70	1.83	1.95	2.00	2.15	2.23	2.29	2.34	2.38	-
- L:	(FPS)	349.	794.	746.	585	23.0	57 K	524	471	417.	364	310.	20.00	207	156.	104.	053	004	956	907.	860.	812.	764.	716.	668.	620.	572.	523	477.	429	5332.R
_	(FT)	50133	49632	40756	66664	42.201	47657	675.10.	47077	466.36	46211	45211	45440	457.00	44737	46477	44217	43619	43603.	43764	42697	4250ce	42075	41624.	41.40	4,655	40045	30622	30008	38555°	138014.8
Σ.	(SFC)	0. 0.	\ \ \ \ \	700		• (1) (1) (4) (4		, 00 C	1 4 1 0 2 4	, (4)		7000	707	764.	7.5	2007	20.7	712	714	716.	8	72.	722	724	726.	1 × ×	730	722	726.	726	1738.0

ST148ET USING ST14MET(11/34), INERTIAL-BI14NO2, NB1C6U DYN. DATA.

•		63.97	65.60	67.27	69.03	70.69	172,328	73.95	75.55	77.12	78.52	80.06	81.61	83.16	84.70	86.26	87.80	89.39	90.99	92.57	60.46	95.37	96.48	97.70	98.86	00.01	01.13	02.28	03.48	04.60	71 71
MACHA	Ĵ	.97	.93	90	.87	.83	4.804	•76	•73	69.	• 66	•62	• 58	• 55	.51	.47	44.	.40	.37	.33	• 5 9	.26	.22	•18	•15	.11	.07	•04	00.	.97	r
	(DEG	4.36	4.14	3.94	3.79	3.65	23.527	3.40	3.26	3.11	2.94	2.74	2.55	2.36	2.16	1.96	1.7ë	1.65	1.51	1.49	1.27	1.91	1.31	9.84	0.64	0.47	0.28	0.10	9.95	9.88	
TAA	(DEC)	03	0.	0	22	13	.209	22	25	22	02	9	12	07	60	07	07	23	47	.01	17	00.	16	.12	02	0	00	0.5	40	10	•
GMA	(DEC)	40.32	30.84	30.00	30.00	39.97	-34.799	36.58	39.88	40.29	41,33	41.09	40.67	40.65	1.10	40.72	40.65	40.61	41.17	36.97	35.93	36.05	36.59	36.45	37.28	38.70	39.80	40.17	C.97	2.12	
90	(DEG)	2.45	1.07	1.40	0.87	0.00	79.700	9.23	8.67	8.10	7.48	6.88	6.20	5.07	5.06	4.45	3.84	3.22	2.61	1.99	1.42	0.80	0.18	9.58	8.39	9.37	7.73	7.09	6.45	5.77	
X.	(056)	3.15	4	2.21	3,74	3.27	-3.299	3.32	3.36	3.39	3.42	3.46	3.49	3.53	3.57	3.60	3.64	3.68	3.71	3.74	3.73	3.71	3.66	3.65	3.65	3.66	3.69	3.73	3.79	3.84	•
VEL	(E52)	.4 60	440	. 400		000	#890 • 1	850	810.	769.	727.	686.	645	605	554.	523.	α 4	443.	403	363	323.	282	240	200	161	121.	083	044	0.07	96 B	•
-	(FT)	1111	20.506	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10410	14026	1183661	17811	17253.	10000	10137	1557a	15018	14457	13897.	13335	12774	12212	11649.	11635	16527	0620	00438	70380	0.03800	67807	67351	4 4 4 4 5	G 8 3 5 .	05744	
1	(SEC)	c c		• ا د ا د د	* 100 C	• a	1 6 0 0 0	• ~ ~ ~ ~				820	200	77.	276		23.0	7.37	7 34	7 7 6	00 00 07 (*) (X (*)	0 4 7		7 7 7 7	4 4	0.00		י מו מו			• • •

ORIGINAL PAGE IS OF POOR QUALITY 214.466 214.446 214.579 214.930 215.723 216.297 216.920 214.361 215.323 214.767 218,198 244 215.275 215.438 218.826 207.976 215.111 219.447 220.167 209. 213. 3,867 3.831 3.794 3.690 3.555 3.522 3.391 3.358 3.228 3.128 3.163 3.163 3.758 3,621 3.587 3.456 3.424 3.326 3.294 3.096 2.996 .724 3.655 MACHA 3 18.243 17.544 17.165 16.626 16.572 16.510 6.132 6.412 19,210 8.815 8.460 16.894 16.144 9.363 8.816 18.667 17,233 17,139 17.024 16.743 16.456 6.238 8,971 16.981 ALPHAA -.057 -.584 -.121 -.142 -.250 -.196 -.154 -.006 -.010 .185 -.733 .045 .218 .278 .248 .893 .301 .210 .087 .177 -,319 -.049 .011 -.322 (050) BFT AA 2.484 2.052 3,813 1.751 -42.096 -41.885 -41.884 -41,330 -40.556 -37.862 -28.446 -8.574 40.953 41.882 44.313 -18.374 064.44 43.142 42.779 40.888 40.250 9.536 6.480 8.616 42,553 43,311 40.122 SIGHAA (DEG) 41.972 62.913 62.239 59.545 59.922 60.473 61,518 60.798 60.177 59.722 59.458 61,206 61.992 62,818 63.692 64.572 69.773 59.404 65,405 66.232 67.173 68.044 68.910 70.644 71.518 72,438 74.281 HDGA (DEG) 73.358 63.63 -4.028 -4.170 -3.616 -3.588 -3.258 -3.230 -4.509 -4.799 -4.175 -4.223 -4.022 -3.381 -3.318 -3,639 -3.817 -4.001 -4.176 -4.343 -4.926 -5.445 3.969 -3.471 -5.045 -5.151 -5.288 -5.603 -4.661 -5.857 (9EC) GAMA 520.7 213.5 315.2 3774.4 3662.8 3485.8 853.3 3814.7 3736.7 3699. A 3626.0 589.7 3553.6 3451.4 3383.4 247.7 179.3 3145.3 3111.3 3042.6 3417.1 3340.4 3231.1 3077.1 3008.0 2973.2 938.B VELA FPS) 04514.0 104744.2 03633.3 03151.1 02618.4 02084.7 00563.9 00114.1 94695 99302.3 98148.6 97317.3 96876.5 9.611996 95947.6 95462.3 64653.6 94455.0 93411.0 .01556.1 01046.0 98921.5 98541.C 97741.1 93937.1 92880.2 92342.1 ALTDE (FT) 0.476 886.0 902.0 TIME (SEC) 862.0 K64.0 866.0 E68.0 570.0 872.0 874.0 1876.0 878.0 880.0 882.0 888°0 890.0 894.0 6.968 0.005 206.2 0.416 1884. 0.268 0.859 608.0 910.0 912.0 916.0 918.0

ST148EF USING ST144ET(11/34), INFRTIAL-BT14NO2, NB1060 DYN. DATA.

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ORIGINAL PAGE IS OF POOR QUALITY

0	(PSF)	03.78	03.13	02.14	00.91	96.96	96.70	94.84	93.47	92.73	95.26	91.65	90.41	88.44	87.07	85.78	84.45	83.36	83.27	84.37	87.19	88.94	89.39	89.58	89.25	89.46	89.86	90.58	91.66	191.983	95.66	
MACHA	3	.30	.28	.25	•23	21	• 18	•16	.13	.11	100	• 08	•00	40.	.02	• 00	66.	97	96	93	46	93	92	6	06	89	88	87	86	.855	84	
I	(0EG)	69.	.67	.54	.52	. 53	.53	. 55	04.	•23	.15	• 05	96.	.71	.57	• 38	.97	.83	. 80	.67	• 84	.62	• 68	. 23	.07	• 76	• 30	.25	.22	206.9	92.	
TA	(DEG)	34	60	.17	42	.13	67	99	03	15	19	22	36	57	87	40	50	57	44	20	28	61	35	7,	17	29	25	.01	.14	121	.12	
CHA	(DEC)	85	.35	1.58	.77	1.30	.87	1.34	4.53	• 10	1.67	1.09	.60	.87	4.50	.57	•66	3.41	2.08	2.81	3.06	3.81	69.9	.83	11.33	2.26	11.85	5.65	63	5.143	.76	
90	(DEC)	2.53	2.50	2.48	2.34	2.45	2.72	2.94	3.04	2.93	2.91	3.02	3.20	3.43	3.90	4.34	4.73	5.24	5.31	5.06	4.79	4.48	4.17	3.44	2.71	1.89	1.15	0.59	0.56	80.933	. 31	
7	(950)	5.15	5,34	, E. C.	5.69	5.88	5.05	5.14	15.14	16.14	15.19	16.26	15.39	16.57	6.83	15.96	17.04	17.19	17.41	17.72	13.00	17.93	17.80	7.56	17.24	17.09	7.07	7.06	7.01	6.93	-17.326	
4	(FPS)	226.	206.		159.	36.	1111	089	990	051.	036.	010	002	984	6.8	5.0	36.	22.	10.	02.	00	910	200	100	7 - 9	53	45.	. α	. 6	76.	318.1	
}- -	(FT)	9621.	7002	465	710	6095	5477	4868	4269	3681	3100.	2526	1958	1305	0835	0276	9725	9178	8636		7536.	7	6446	5007	7220	1000	100t	- 00 a c	9040	• 0000	42440.0	
I	(SEC)	9	• • • • • •	• • • •	• 4 • 4 • 6	, de		5.50	054	5.5	0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	090	062	4			020	072	.740	7.0			י מי מי) (4)	• 4 • 4 • 0				• V V		26.98	

2	-	ũ	E	90	A M	V L	PHA	U	
SEC)	(FT)	(FPS)	(DEG)	(DEG)	(DEG)	(DEG)	(066)	<u> </u>	(PSF)
ć	0 9	3	7.81	1.85	0.15	•	.41	*	94.11
	41449 B	808.6	, 70 4 	82.462	11.066	526	6.637	.834	195.849
1 4	0946	40	3.29	3.20	0.32	8	•76	2	97.97
	442.	01.	3.28	3.82	7.46	•37	.79	2	00.35
8	9941.	97.	8.28	4.30	• 48	8	• 75	~	02.14
5	0444	91.	8.21	66.4	.98	11.	.59	0	03.02
2	8950.	36.	8.24	5.48	.37	~	• 59	0	04.04
•	8401.	80.	8.21	5.30	.45	3	. 50	0	04.84
	7975.	76.	8.23	4.62	11.85	.11	•51	8	06.29
6	7439.	73.	3.36	3.10	18.80	74	.33	8	08.81
•	7001.	70.	8.58	1.39	19.50	•10	.37	~ i	10.01
2	650B.	90	8.89	9.48	25.17	00	. 53	~	12.31
4	6010	61.	9.28	65.9	3.12	•	. 88	9	13.58
•	5503.	55.	9.85	3.87	38.12	0	66	5	14.32
	4437.	51.	3.27	0.43	38.85	-	.67	5	15.61
0	4460.	46.	3.55	6.62	43.46	œ	• 86	4	17.11
2.	3441.	42.	0.93	2.47	45.35	5	• 20	3	18.44
4	3409	37.	21,36	7.81	48.23	25	• 56	m	19.57
ģ	2873.	31.	21.66	2.71	8.85	4	.79	2	20.27
00	2335	26.	1.69	7.59	42.34	m	• 75	~ [21.33
0	1795.	21.	2.12	2.50	7.08	0	. 80	-	22.50
2	1254.	17.	22.25	7.20	46.71	~	• 84	0	23.70
4	0716.	10.	2.30	1.88	5.55	W.	.79	O:	23.50
	0183.	02.	2.32	68.9	41.47	ω	.80	œ	22.61
000	9657	97.	2.15	2.22	9.53	8	647	100	23.03
0	9139.	92.	1.88	7.93	4.83	2	.34	~	23.89
	8633.	80	1.47	• 16	32.36	0	96.	9	24.74
4	8137.	84.	1.27	.72	1.40	•	96.	•	25.65
•	7651.	81.	20.85	.35	30.22	3		5	27.29
) I (•				•		į	

1											•												ŧ							1	
0 A (PSF)	31.25	32.30	32.73	33.69	33.55	233.084	32.57	31.65	30.32	29.00	27.43	25.13	24.29	25.61	26.36	27.43	28.36	28.20	27.80	26.97	25.78	24.30	22.42	19.96	17.28	13.26	09.19	05.26	01.66	06.00)) •
MACHA (-)	65	99	49	63	63	.625	61	9	9	09	50	58	8	57	57	~	56	56	56	5	55	3.4	34	53	53	52	52	51)
ALPHAA (DEG)	85	45	.37	•64	32	8.179	10	112	.14	.62	69.	•24	.80	00.	61	64.	.79	.32	.70	.47	.36	. 65	.82	.71	92.	.21	96	.97	3.7	70	•
RETAA (DEG)	. 42	4	50	33	46	. 553	56	43	50	69	43	26	26	32	41	50	65	40	40.	35	.31	.08	0	90	E	26	35	40	`	· •C	~
SIGHAA (Deg)	33,36	34.65	34.74	34.65	33.79	-33.818	33.99	35.18	36.33	38.82	40.69	40.04	41.12	39.01	38.35	36.58	34.59	33.46	29.81	27.26	26.42	26.68	27.73	27.88	27.08	26.83	27.09	26.53	27.72	,	7 * * * 7
HD GA (DE G)		3.61	7.59	1.89	6.03	-20.030	3.98	8.18	2.42	6.95	1.86	7.14	2.47	7.38	2.55	7.47	2.20	7.04	81.49	85.24	88.71	92.01	95.55	90.24	02.92	06.55	10.61	12.21	1 6		70.61
GAMA (DEG)	44	7.50	.0	9,49	3.75	-13,432	91.4	17.86	7.77	17.73	17.76	17.65	17.46	7.62	17.05	6.46	15.67	16.67	13.72	2.0	12.01	11.44	10.79	0.18	10.56		, K	77.0		- [7.
VELA (FPS)	767	700	0		• •	656.2	31.0	, , , , ,	0 0	7 0	0	, ,	17.	15.	, (r	, , , , , , , , , , , , , , , , , , ,	0	9			• 4	000	7 6	, c	77.	- (, n			٠ د د	45
ALTDE		60044	5 7 7 F	F 200	, UCC.	0.26342	40,40	2670	2000	3 F 5 F 6	2514	2126	1765	3000	1020	1000 047x	2460		0000	0452	0107	0043	04770	0 1 1 0	• 010°	03160	7057		- 2 C . C	(625)	7447.
TIME		001	. 70T	104	9001	2120	1	. 7	114	- a	0 C		707	186			100	. 70	174	000	• 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• 0000	. 700		0000	• 0 • 0 • 0 • 0	• c t c	.777	214.	510.	218.

IME ALT SEC) (FT 2000 1724									
20.0	ë VEL (FPS	A GAMA (DEG)	HDGA (DEG)	SIGMAA (DEG)	BETAA (DEG)	ALPHAA (DEG)	MACHA	0A (PSF)	1
	545	-11.35	-122.69	32.78	24	• 66	•	98.28	
22.0 1701	540	.9 -12.82	4 -126.300	-34.561	.370	8.322	964.	198.153	: 1
224.0 16766	.6 539	.4 -13.93	-130,19	34.29	27	.47	64	98.53	
200 1649	6 538	.5 -14.98	-134.16	34.73	24	.92	0	99.44	
28.0 1620	3 536	.9 -15.77	-138.33	34.88	17	• 11	0	96.66	à
	7 537	.0 -16.24	-142.96	35.65	.31	.45	O	01.75	
37.0 1560	.4 537	.8 -16.29	-148.40	36.71	.05	• 04	0	04.18	
34.0 1529	.2 540	.2 -15.27	-153.77	34.71	.36	.75	65	07.82	. (
36.0 1493	0 543	-16.65	-158.49	37,31	.41	•62	40	12.25	
38.0 1466	0 549	.2 -17.79	-163.13	36.45	•38	.74	20	18.88	
46.0 1431	.2 557	.7 -18.73	-167.52	31.50	.77	.30	20	27.98	
45.0 1394	.5 565	.7 -19.16	-171-43	29.35	.14	• 28	27	37.12	1
44.0 1355	.5 573	.0 -19.26	-174.74	21.51	1.16	• 04	52	45.97	
46.0 1318	.6 578	.3 -13,16	-176.60	12.04	.08	.24	52	53.32	
43.0 1280	.3 583	. P -13.63	-177.74	4.52	O.	• 35	2	61.05	
50.0 1243	.7 591	.5 -18,15	-178.43	1.35	.85	.74	50	70.857	•
52.0 1205	6 594	.4 -17.97	-178.25	7.48	.72	.85	5	76.50	םר
54.0 1169	6 593	.4 -17.82	-177.26	8.86	.81	.32	53	78.521	10
56.0 1134	583	8 -15.13	-175.42	1.10	.25	.24	52	72.309 0	rn e
58.0 1103	. 573	.6 -14.57	-173.50	•38	•01	.41	21	65.291 2	A = :
60.0	564	.2 -14.21	-172.23	6.94	.39	• 61	50	58.729	_
62.0 1046	9 557	9 -14.60	-171.73	27.	45	• 78	0	55.1010	
64.0	3 556	.6 -15.12	-171.90	2.75	07	.91	49	56.108P	1
480 084	.3 557	.5 -15.91	-171.86	.15	33	.32	49	59.347日	
68.0 951	9 559	2 -17.35	-172.03	2.36	70	.47	0	63.451	i
70.0 917	1 562	.4 -17.10	-172.19	09.	52	94.	0	69.05	ļ
72.0 884	7 559	.5 -16.79	-171-73	.39	48	.37	40	68.90	
74.0 852	5 554	.8 -17.23	-170.97	48.	.00	.01	49	66.88	
70.0 814	7 547	.2 -17.67	-169.91	_	-	. 48	8	62.13	. :
78.0 784	945	.1 -17.91	-169.80	.23	.61	.72	48	61.77	

3

	- - - - -						Commission of the Commission o	M. M. COLO. C. Dr. C. Shiphing (McGregory (March)) in the co.)
TIME (SEC)	ALTDE (FT)	VELA (FPS)	64MA (0E6)	HDGA (DEG)	SIGMAA (DEG)	BETAA (DEG)	ALPHAA (DEG)	4AC#A	0A (PSF)
77	7	26.	0	169.22	80	60	.32	8	11.6
240	100	- 4 - 4		169.19	96.	24	.51	27	3.0
366	101	80		169.31	99	33	.70	56	93.1
366	102	72.		169.40	E	27	3.70	23	7.5
7348.0	2102.0	252.4	300	-169,189	.626	.542	-3.801	.221	66.68
350	102.	38		169.10	4	31	3.64	20	Q.
352	101.	25.	0	168.75		96	3.65	57	
354	101.	6	N	169.46	0	47	3.63		7.6
356.	101.	01.		170.25	S	16	3.64	11	2.31
358	101.	89.	0	170.59	5	43	3.72	9	7.5
300	101.	78.	œ	170.31	0	34	3.71	1	3.2
362.	130.	67.	(1)	169.84	0	0	3.69	7[9.5
364.	100.	55.	7	170.07	O	•	3.69	(T)	5.5
366	130.	44.	8	170.38	~	84	3.67	71	1.7
368	130.	31.		170.48	m	O	3.75	ا جنم ابنتم	8
370.	100.	17.	0	170.18	2	•	3.73	C)	
372.	0.660	.90		169.75	0	3	3.73	3	1.7
374.	.660	96	-	169.65	(C)	m	3.71	0	9.6
376.	.060	•		169.83	Q.		3.73	6	a o .
373.	660	~		169.63	0		3.81	9	ا الم ا
380	900	8		170.12	œ	m	3.73	90	0
382.	0.48	•		170.31	-4	0	3.65	S)	~
364.	.960	٠ د		170.03	\sim	37	3.73	40	Ø 1
386.	634.	9		170.09	3	-	3.55	Ť	N
388	698.	•		160.691	Ó	17	3.67	M	
396	097.	•		169.77	9	32	3.57	N	
392.	097.	5	.35	169.74	~	4	3.35	5	NI i
394.	C97.	ω. •	3.65	171.54	•88	1.19	05	0	~
396.	097.	•	59.43	76.92	B	_	**	a	0
398.	697.	•	3.02	-5.91	4.47	4.68	2.77	9	

STI48ET USING STI44ET(11/84), INFRTIAL-BT14NO2, NB1060 DYN. DATA.

IME SEC)	ALTDE (FT)	VELA (FPS)	6 4 4 A (DEG)	HDGA (DEG)	SIGMAA (DEG)	8ETAA (DEG)	ALPHAA (DEG)	MACHA	0A (PSF)
0,		•	1.37	7.66	29.133	.03	9	000	0
, °	900		62.6	54	8.06	_	6.41	000	000.
			63.09	25.68	62.46	8.84	6.49	0000	O
	960		2.50	6.52	0.45	3.94	2.97	000•	0
800	1000		62.13	36.52	0.01	1.25	8.94	000.	0
			1.46	49.33	39.085	.14		000	0
2	1.45		67.68	46.17	1.55	4.43	9.92	0000	0
7	360		65.88	31.32	6.39	8.79	3.86	000	0
	094.	} ~	3.27	39.05	96.9	E	6.62	0000	0
000	760		63.23	39.85	96.	5.72	2.05	000	0
0	450		59.20	34.35	1.47	4.19	7.83	99C•	0
2 2	0.33		5.12	42.70	4.69	6.49	9.70	0000	0
7	660		60.04	42.73	 8	-20.109	5.07	000.	000.
26.	.093		59.79	4.67	51,299	3.63	8.09	000	0
S 2	43	• 5	59.20	45.21	.20	0.98	5.69	000	0

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APPENDIX D

STS-14 (41-D) Source and Output Products for Archival

D.1 STS-14 Output Products

(a)	FILES

NAME	USER CATALOG	DESCRIPTION
BT14N02	169750N	Final reconstructed trajectory (40 word format per AMA 81-1)
ST14BET	274885C	Final extended BET (66 word format per AMA 81-11)
NAVB41D	389102C	STS-14 onboard nav BET (66 word format)
ST14MET	712662N	Final LAIRS file
TRWS41D	274885C	Reformatted JSC/TRW BET (66 word format)
IMRGA14	274885C	Signal difference file (IMU2 - RGA1/AA1)

(b) TAPES

REEL NO.	DESCRIPTION
NB1248	STS-14 AEROBET (201 words per AMA 82-9)
NC0601	Duplicate of above
NW0766	25 Hz IMU2 GTFILE (62 words per AMA 81-20)
NR0101	25 Hz RGA1/AA1 GTFILE (62 words per AMA 81-20)
NE0716	25 Hz RGA1/AA1 for NR0101
NR0116	25 Hz bias rectified RGA1/AA1 file for GTFILE generation
NB0946	Final STS-14 residuals for BT14N02
NC0943	Edited tracking tape
NB1056	1 Hz OI-2 for AEROBET
NB1060	20 Hz IMU2 file in body axes for ST14BET, AEROBET, and GTFILE (calibrated per BT14N02 solution)
NB0945	Dynamic data (input for trajectory reconstruction)- 20 Hz IMU2 data in platform coordinates (second CDC record)

D.2 Source Tapes Received via NASA LaRC

(a) T/M TAPES

REEL NO.	DESCRIPTION
NA0930	OI-1
NB1202/NC0110	OI-2
NA1015	OI-3 (source for RGA1/AA1 data)
NA1004	OI-4
NU1207/NU1277	OI-1 from CBET1F

(b) TRACKING TAPES

REEL NO.	DESCRIPTION
NU0927	JSC/TRW tracking data
NT0571	Goddard Space Flight Center data
JH41D4	AFFTC theodolite data

(c) OTHER

REEL NO.	DESCRIPTION						
NB0833	JSC/TRW Descent	BET					
JH41D1	Jimsphere data	(balloon	1;	landing	-	1 ½	hours)
JH41D2	Jimsphere data optical track)	(balloon	2;	landing	+	30	minutes;
JH41D3	Jimsphere data radar track)	(balloon	2;	landing	+	30	minutes;



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16. Abstract

Trajectory reconstruction results for the first Discovery flight are presented. Spacecraft dynamic measurements from IMU2 were utilized in conjunction with the ground based tracking data from two S-band stations, eight C-band, and five cameras at Edwards Air Force Base to determine the spacecraft trajectory from epoch through rollout on Runway 17. Specifics as to the trajectory reconstruction are discussed in Section I herein. The final inertial profile is BT14N02/UN=169750N. Merging of this file with the final LAIRS atmosphere is discussed in Section II. The final Extended BET is ST14BET/UN=274885C. Section III presents plots of relevant parameters from the AEROBET as well as aerodynamic performance comparison results. High frequency files for maneuver extraction were also generated as discussed in Section IV. Appendices are attached which contain (A) spacecraft and physical parameters utilized, (B) final residuals obtained from the data fitting process, (C) listing of trajectory parameters, and (D) archival information.

17. Key Words (Suggested by Author(s))

Space Transportation System, Best Estimate Trajectory, aerodynamic comparisons, atmosphere evaluations

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